

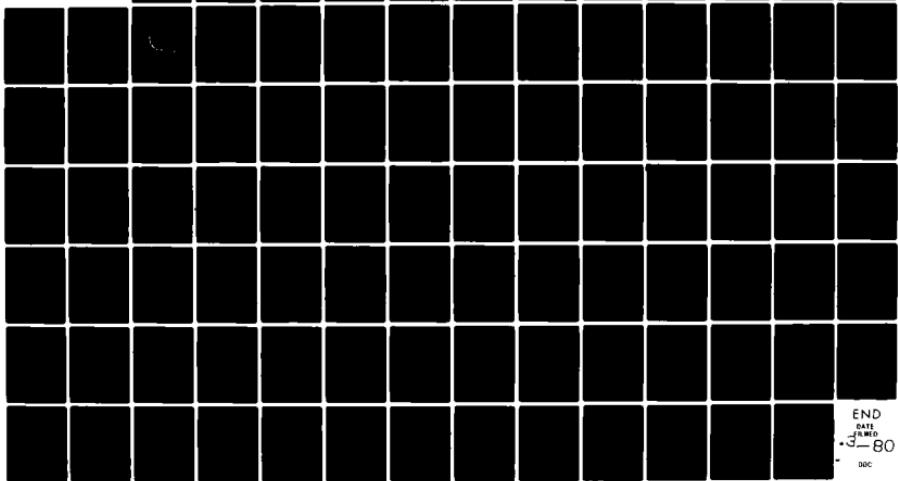
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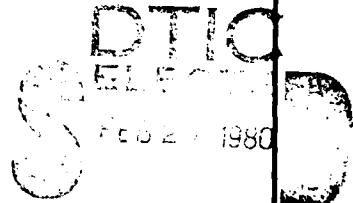
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FINITE ELEMENT ANALYSIS OF PIPE ELBOWS

by

Melvyn S. Marcus and Gordon C. Everstine

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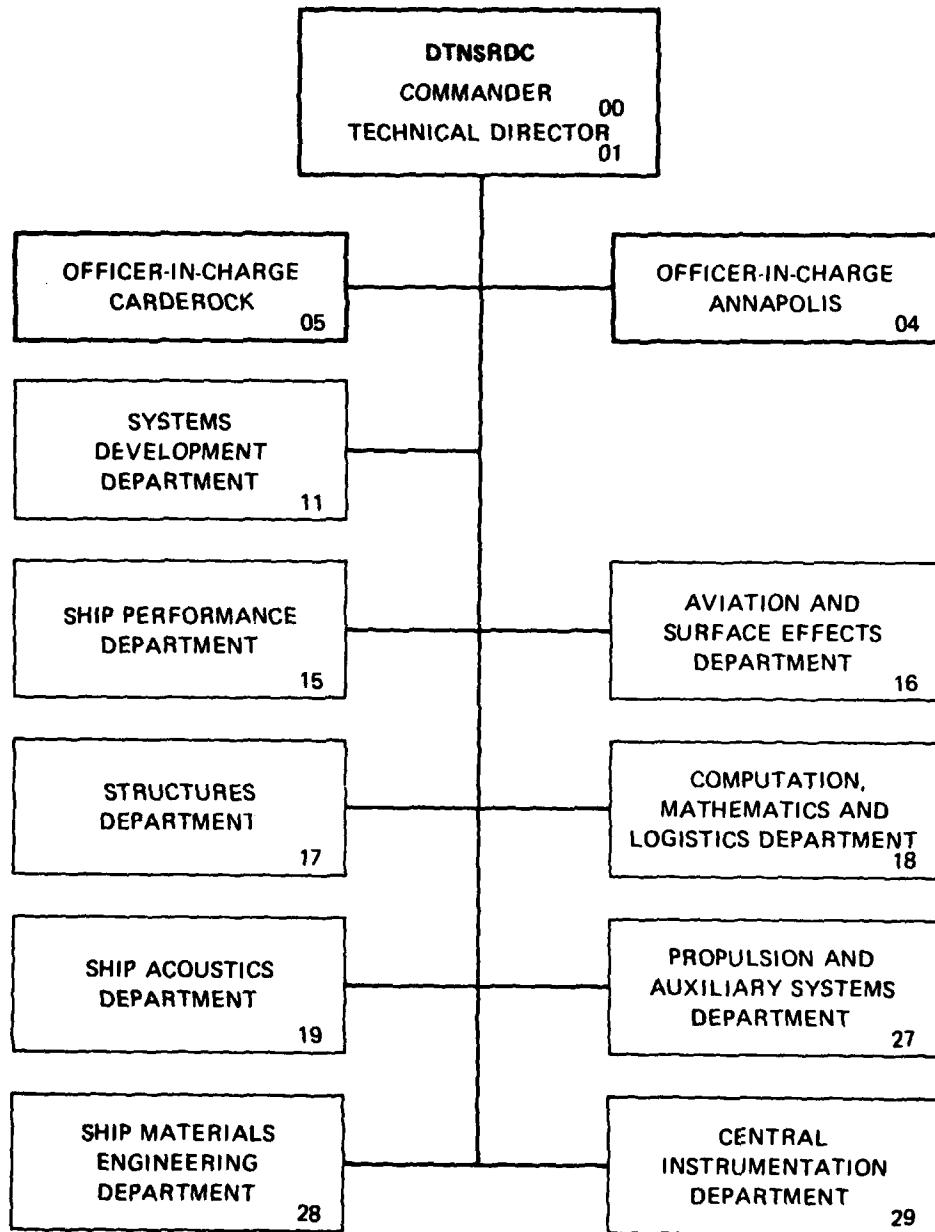
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Computer runs to automatically generate NASTRAN input data, execute NASTRAN, and postprocess NASTRAN output are included. A sample NASTRAN data input file is also listed.

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ABSTRACT

NASTRAN analyses were performed with three different finite element models on a 90-degree pipe elbow to determine principal stresses due to internal pressure, inplane bending, out-of-plane bending, and torsion moment loadings. Comparison with stresses experimentally obtained under the four loading conditions demonstrates the adequacy of a finite element model with ideal geometry assumptions and an economical mesh spacing. Implementation of the NASTRAN modeling is described in detail. Deck set-ups for a sequence of computer runs to automatically generate NASTRAN input data, execute NASTRAN, and postprocess NASTRAN output are included. A sample NASTRAN data input file is also listed.

BACKGROUND

The objective of one of DTNSRDC's programs is to reduce the size and weight of sea-water piping systems sufficiently to achieve the design goals. This objective can be accomplished in several ways: (1) by using higher strength materials, (2) by improving fabrication techniques, (3) by better designs, and (4) by less conservative structural acceptance criteria and stress factors. The third and fourth alternatives require the application of more refined structural analysis methods such as the finite element method (FEM). With the FEM, the analyst can gain a more accurate understanding of general end point motions, which influence piping system designs, as well as of motions and stresses in the piping systems themselves.

The design of piping systems depends on a knowledge of the stresses and deflections of the pipes due to the anticipated service loads. In general, these loads may be either static or dynamic. The static category includes pressure, moment, and thermal loads; the dynamic includes shock loadings. For any of these loads, the most critical locations are usually in components such as elbows and tees. It is well known, for example, that a curved pipe does not respond to bending loads in the way predicted by elementary beam theory, which is usually adequate for straight pipes.

This report describes finite element analyses of piping elbows subjected to both pressure and moment loads. The NASTRAN finite element structural analysis computer program was used. Stresses and flexibility factors were computed, and the stresses were compared to experiment. The two main purposes of the work were:

- (1) to determine modeling conditions (including mesh size and ideal geometry assumptions) for which a NASTRAN finite element analysis of the pipe elbow would yield results in good agreement with experiment, and
- (2) to provide deck set-ups for NASTRAN data generation and solution implementation which could be used to automate a computerized parameter study of pipe elbows.

Such a study, for example, could yield basic information on the structural behavior of elbows. Also, given the increased accuracy and reliability attainable with finite element models, compared to the less precise traditional methods, the studies could be conducted in accordance with less conservative design rules similar to those of the ASME Section III nuclear pressure vessel code.

STATEMENT OF THE PROBLEM

The structure to be analyzed is the 10-inch, schedule 40, 90-degree carbon steel pipe elbow referred to as ME-1 by the Reactor Division of the Oak Ridge National Laboratory.^{1*} This elbow, one of four machined at Oak Ridge to test the effects of thinning and ovalling, was machined so as to simulate as far as possible an elbow with ideal (uniform) geometry. Details on the geometry of ME-1 are shown in Figure 1. Oak Ridge also

*A complete listing of references is given on page 25.

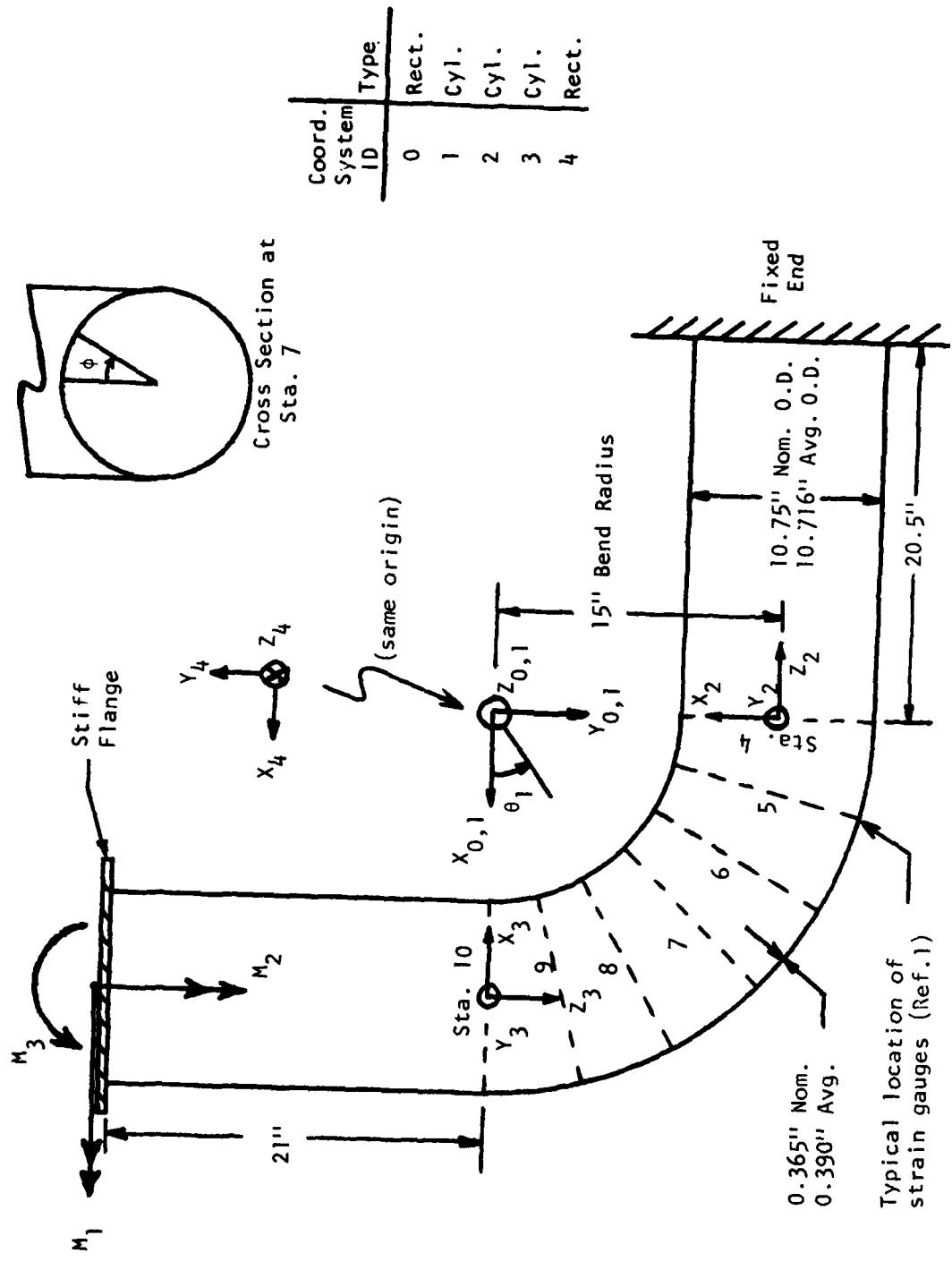


Figure 1 - Geometry and Coordinate Systems of Pipe Elbow ME-1

made measurements of the actual wall thickness and elbow diameter for the test model; these measurements are listed in Tables 1 and 2, respectively. All values in each table were averaged to obtain the average wall thickness and outside diameter values of 0.390 inch and 10.716 inches, respectively. Thus the average value of mean radius (to middle of wall) is 5.163 inches.

This elbow structure was subjected to four different loadings:

- (1) internal pressure of 75.53 psi
- (2) in-plane moment of 32,660 in-lb ($M_3 = -32660$ in Figure 1)
- (3) out-of-plane moment of 32,660 in-lb ($M_1 = 32660$ in Figure 1)
- (4) torsional moment of 32,660 in-lb ($M_2 = 32660$ in Figure 1)

These loads were also used for the analysis.

The material properties of carbon steel are $E = 2.9 \times 10^7$ psi (Young's modulus) and $\nu = 0.3$ (Poisson's ratio).

THE NASTRAN MODELS

Three analyses were performed:

Mesh A -- a uniformly spaced mesh of finite elements (Figure 2) for an ideal (uniform geometry) elbow having the same thickness and diameter throughout; the values used for the wall thickness and middle radius were the mean values computed from Tables 1 and 2: 0.390 inch and 5.163 inches, respectively.

Mesh B -- similar to Mesh A except that the number of elements in each direction was increased by 50%.

Mesh C -- a uniformly spaced mesh of finite elements for the actual elbow ME-1 as measured and tabulated in Tables 1 and 2; the mesh spacing was the same as for Mesh A, the coarser of the two idealized models.

For the ideal models (Meshes A and B), the structure is symmetric with respect to the plane $Z_0 = 0$ in Figure 1, so that only one-half of the structure need be modeled. Although the actual geometry used for Mesh C does not exhibit the same symmetry, such symmetry was assumed here also, and only half the structure was modeled. This assumption is equivalent to assuming that the nonsymmetry in the thickness variation on the unmodeled side ($Z_0 < 0$) has little effect on the solution on the modeled side

TABLE 1 - MEASURED VALUES OF WALL THICKNESS FOR ME-1

ϕ (degrees)	Wall Thickness (in inches) at						St. 9	St. 10
	St. 4	St. 5	St. 6	St. 7	St. 8			
0	0.395	0.389	0.404	0.402	0.384	0.388	0.381	
22.5	0.394	0.392	0.401	0.399	0.384	0.393	0.391	
45.0	0.394	0.389	0.406	0.401	0.381	0.378	0.398	
67.5	0.398	0.398	0.396	0.398	0.385	0.376	0.401	
90.0	0.396	0.397	0.398	0.404	0.386	0.392	0.392	
112.5	0.394	0.383	0.386	0.393	0.381	0.379	0.385	
135.0	0.395	0.375	0.382	0.393	0.384	0.378	0.381	
157.5	0.394	0.380	0.382	0.393	0.379	0.384	0.380	
180.0	0.390	0.389	0.388	0.383	0.386	0.386	0.380	
202.5	0.396	0.391	0.388	0.389	0.389	0.391	0.387	
225.0	0.395	0.380	0.382	0.386	0.402	0.392	0.397	
247.5	0.394	0.366	0.372	0.374	0.389	0.383	0.387	
270.0	0.396	0.381	0.406	0.401	0.391	0.406	0.401	
292.5	0.390	0.383	0.393	0.390	0.390	0.394	0.394	
315.0	0.390	0.384	0.394	0.383	0.391	0.389	0.394	
337.5	0.391	0.382	0.399	0.406	0.395	0.388	0.390	

TABLE 2 - MEASURED VALUES OF OUTSIDE DIAMETER FOR ME-1

ϕ (degrees)	St. 4	St. 5	St. 6	St. 7	St. 8	St. 9	St. 10
0	10.765	10.729	10.730	10.705	10.735	10.750	10.787
22.5	10.765	10.735	10.720	10.725	10.710	10.741	10.797
45.0	10.738	10.700	10.690	10.717	10.685	10.705	10.759
67.5	10.738	10.677	10.671	10.690	10.664	10.677	10.700
90.0	10.700	10.680	10.672	10.680	10.660	10.690	10.681
112.5	10.713	10.680	10.675	10.695	10.694	10.716	10.732
135.0	10.735	10.695	10.685	10.707	10.715	10.728	10.762
157.5	10.758	10.703	10.713	10.740	10.737	10.745	10.807

Average O.D. = 10.716 in.

($Z_0 \geq 0$). Since a deliberate attempt was made to machine the ME-1 model to minimize thickness variations, this is probably a reasonable assumption.

For all three meshes, the elbow and its adjoining straight sections were modeled with flat plate finite elements (the NASTRAN element QUAD2) which have both membrane and bending stiffness. As indicated in Figure 1, one end was completely fixed, and the other end (where loads are applied) was connected to a stiff flange (which was assumed to be rigid in the finite element model).

The bulk of the NASTRAN data deck for each model was generated by a computer program called PIPELB, described briefly in the next section.

The finite element (QUAD2) used in these models yields stresses at element centroids. Hence, to facilitate comparison with experiment at the middle of the elbow ($\theta = 45^\circ$), an odd number of elements was used in the longitudinal direction.

Figure 2 shows the Mesh A finite element model. This plot was generated using the Structural Analysis via Generalized Interactive Graphics (STAGING) system.²

The characteristics of the three meshes are summarized in Table 3. In all three cases, the element aspect ratios within the elbow were selected so as not to deviate significantly from unity, which is the optimum aspect ratio for the QUAD2 finite element.

THE DATA GENERATOR

The computer program PIPELB was written to generate NASTRAN data for THETA-degree elbows of ideal or non-ideal geometry adjoined on both sides by straight sections of arbitrary length. In addition to the GRID cards, which locate the finite element mesh points, the program also generates the plating (NASTRAN data card CQUAD2), pressure loading (PLOAD2), symmetry and other constraints (SPC), and flags for congruent elements (CNGRNT). As added conveniences, PIPELB will automatically generate the set of element identification numbers (ID's) for the mid-THETA elements which constitute the solution set for stresses; flexible spokes (CBAR) radiating from the centers of both elbow end-circles which facilitate the

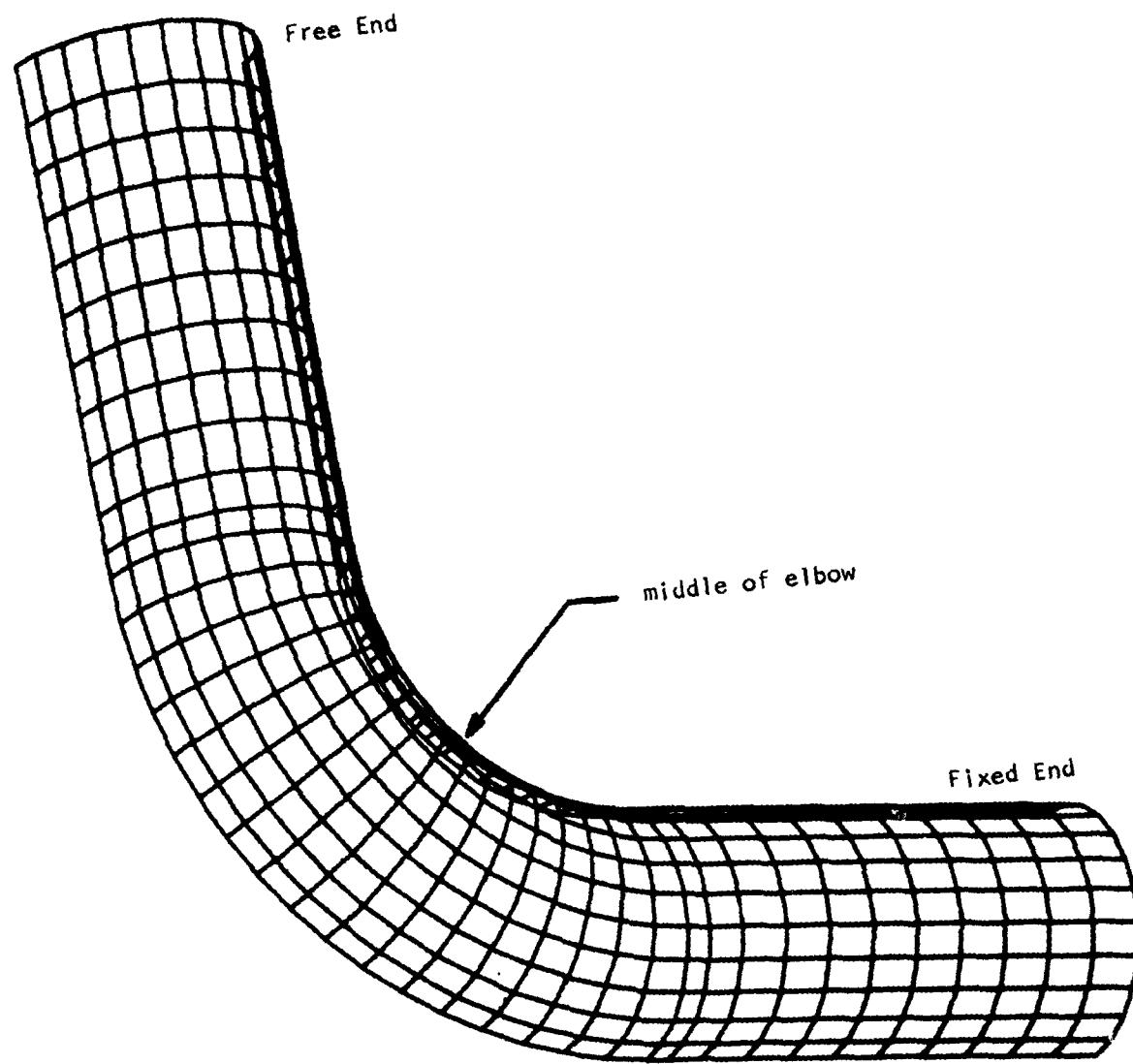


Figure 2 - Finite Element Model of Elbow (Mesh A)

TABLE 3 - SUMMARY OF FINITE ELEMENT ANALYSES

Structure Being Analyzed: Pipe Elbow ME-1 (See Figure 1)

Modeling and Computational Parameters		Mesh A	Mesh B	Mesh C
Ideal or actual geometry	ideal	ideal	ideal	actual
Mean radius of pipe	5.163 in.	5.163 in.	5.163 in.	see Tables 1,2 see Table 1
Thickness of pipe	0.390 in.	0.390 in.	0.390 in.	see Tables 1,2 see Table 1
No. of elements in circumferential direction	12	18	12	
No. of elements longitudinally spanning 90° elbow	17	27	17	
No. of elements longitudinally spanning 21.0° straight section	11	16	11	
No. of elements longitudinally spanning 20.5° straight section	11	16	11	
Total number of elements	468	1062	468	
Number of grid points	520	1140	520	
Number of degrees of freedom	2745	6273	2745	
Average matrix wavefront	79	116	79	
NASTRAN CP time (CDC 6400)	949 sec.	2850 sec.	1339 sec.	

computation of flexibility factors; a rigid element (CRIGDI) at the free (loaded) end of the pipe; and the end cap longitudinal load (FORCE) due to unit internal pressure.

The data generator defines grid locations within the elbow section in terms of a local cylindrical coordinate system (ID number 1 in Figure 1) defined by

$$\begin{aligned} R &= RBEND - RPIPE \cdot \cos \phi \\ T &= \theta_1 \\ Z &= RPIPE \cdot \sin \phi \end{aligned} \tag{1}$$

where RBEND is the elbow bend radius measured to the pipe centerline, RPIPE is the mean pipe radius, ϕ is the angle spanning the pipe half-circumference, and θ_1 is the angle spanning the elbow arc of THETA degrees. (Other coordinate systems used in the NASTRAN data deck are defined in Figure 1.) The grid marking system defines the grid ID's as

$$\text{GRID ID} = 1000 \cdot (500 + ITH) + IPH \tag{2}$$

where ITH and IPH are θ_1 and ϕ , respectively, rounded to the nearest integer. The element ID assigned to each quadrilateral is equal to the GRID ID that would be assigned for a node located at the element centroid.

For example, for Mesh A, the elbow was modeled with 17 elements covering the 90° elbow arc longitudinally (i.e., a spacing of 5.294°) and 12 elements covering 180° (i.e., a spacing of 15°) in the circumferential direction. Thus, for this mesh, point 51100 is at the intrados (the inside edge), 511090 is at the top, and 511180 is at the extrados (the outside edge) of the elbow, with all three points at $\theta_1 = 10.588^\circ$.

The shell was modeled with plate elements (NASTRAN data card CQUAD2). Symmetry constraints were applied with SPC's at $\phi = 0^\circ$ and $\phi = 180^\circ$. An internal pressure loading was specified using a PLOAD2 card for each plate element, and the resultant longitudinal load at the closed free end (due to the pressure) was specified with a FORCE card. The inplane bending, out-of-plane bending, and torsion moment loads were applied at the rigid flange at the free end using MOMENT cards. All grid points at the fixed end were constrained in all six degrees of freedom.

Appendix A provides a listing of the card deck needed to create an UPDATE program library, compile source code, and catalog executable code for the data generator PIPELB.

Appendix B gives a listing of a typical card deck needed to execute the data generator and create a data file suitable for input to NASTRAN. The specific example used in Appendix B is for Mesh A. The result of executing this step is the NASTRAN data deck, which is listed in Appendix E. Various sections of this data deck have been labeled with comment cards, which have a \$ in card column number one.

For Mesh C, which uses the measured geometry as listed in Tables 1 and 2, the data generator interpolates to obtain pipe thicknesses at element centroids and to obtain pipe radii at the grid points. This interpolation is performed within the generator in subroutine FIND. For Mesh C, each element has a unique thickness and hence a unique property card (PQUAD2).

SOLUTION SEQUENCE

The general computational approach is to perform the following steps:

Step 1: Compile the elbow data generator, and catalog an executable form of the program. See Appendix A.

Step 2: For the desired mesh, execute the generator, and create and store the NASTRAN data deck. See Appendix B.

Step 3: Using the data deck created in Step 2, execute NASTRAN and save (on a permanent file) the stresses at the desired location ($\theta_1 = 45^\circ$).

See Appendix C for a listing of control cards to accomplish this.

Step 4: Smooth the stress curves in preparation for plotting, storing the results. Figure 3 shows a typical plot of the type desired, where various stresses at the section $\theta_1 = 45^\circ$ are plotted as a function of ϕ , the circumferential coordinate. As can be seen in Figure 3, the smoothing merely provides a more attractive display of the results. The smoothing in Figure 3 was obtained by using the B-spline³ application subprogram CRVFIT.^{4,5} See Appendix D for a listing of the deck to read the NASTRAN principal stresses and perform the smoothing.

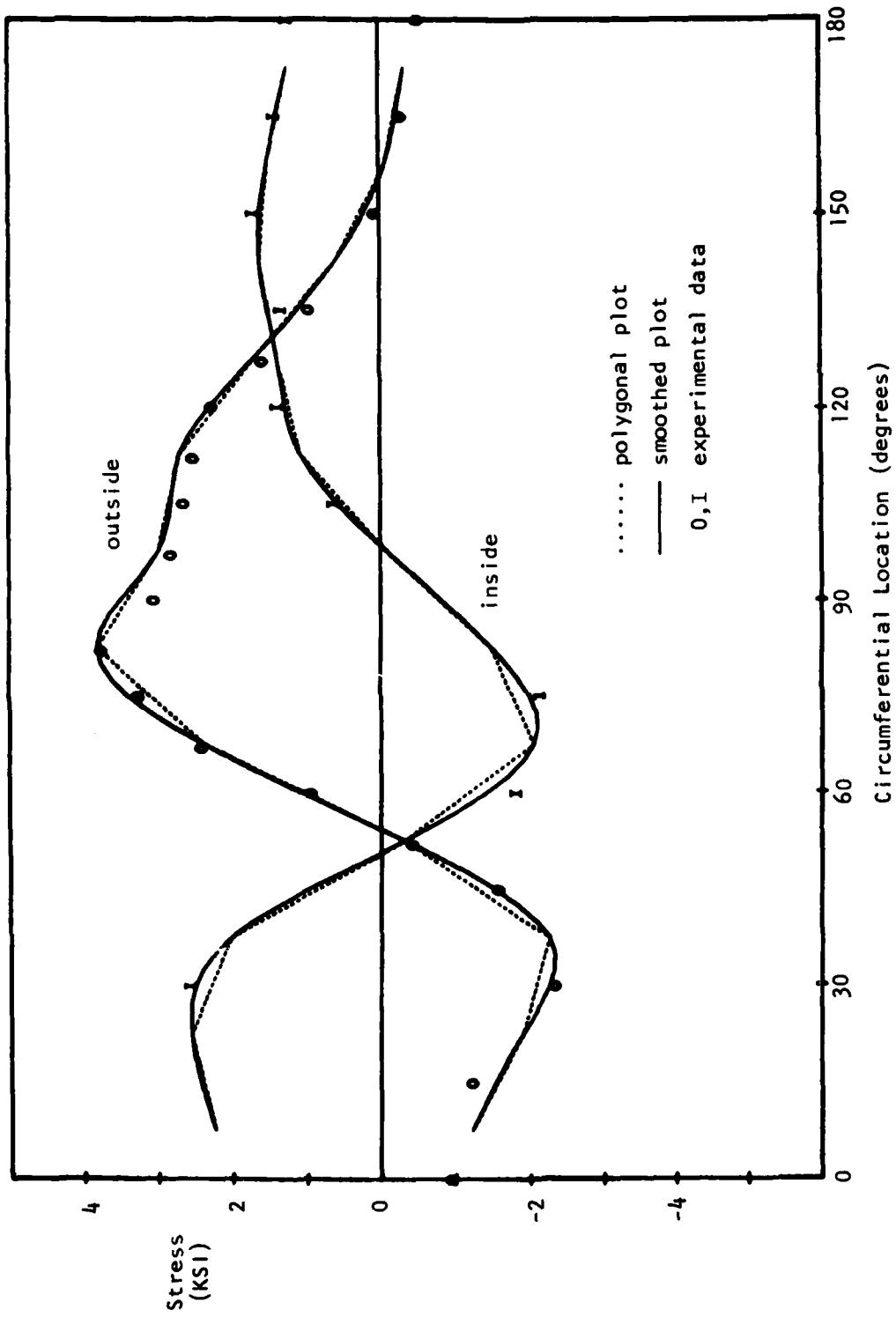


Figure 3 - Comparison of Polygonal and Smoothed Plots of Major Principal Stress at Middle of Elbow Due to Inplane Moment Load (Mesh A)

Step 5: Plot the smoothed results using the informally documented interactive computer graphics package PLOT QUICK developed by Mr. Melvin E. Haas of DTNSRDC (Code 1843).

FLEXIBILITY FACTORS

The finite element models also allow for the convenient determination of flexibility factors, which are of vital interest to piping systems designers. To avoid confusion, the term "flexibility factor," as used in this report, will be defined precisely. The flexibility factor k of a piping component is defined as the ratio of a relative rotation of that component to a nominal rotation:

$$k = \frac{\theta_{ab}}{\theta_{nom}} \quad (3)$$

where

θ_{ab} = rotation of end "a" of the piping component relative to end "b" of that component due to a moment loading M , and in the direction of M .

θ_{nom} = nominal rotation of an equal length of straight pipe due to the moment M .

For elbows, the nominal rotation is computed using simple beam theory, in which case one obtains

$$\theta_{nom} = \frac{ML}{EI} \quad (4)$$

for inplane and out-of-plane moments, and

$$\theta_{nom} = \frac{ML}{GJ} \quad (5)$$

for torsional moments, where

M = applied moment load

L = arc length of elbow

E = Young's modulus of material

G = shear modulus of material

I = moment of inertia of cross-section

J = torsional constant of cross-section (equal to the polar moment

of inertia for circular cross-sections)

For 90° elbows, $L = \pi R/2$, where R is the bend radius.

The determination of the relative rotation θ_{ab} from the finite element model is complicated by the fact that plane cross-sections do not remain plane after deformation, so that each point on the surface of the shell has a different rotation. However, an "average" rotation for a cross-section may be obtained by connecting very flexible beam spokes from each shell grid point to a new grid point located at the center of the circular cross-section. The rotation of this center point may be used as the average rotation for the cross-section. For Mesh A, the center point at Station 4 in Figure 1 is labeled 590500 (end "a") and at Station 10, 500500 (end "b").

Table 4 shows the details of the flexibility factor calculations for the three moment loads for Mesh A.

RESULTS AND DISCUSSION

Principal stresses were computed by NASTRAN at the middle of the elbow ($\theta_1 = 45^\circ$) and compared to experimental results obtained at the Oak Ridge National Laboratory.¹ These stresses were computed for four separate loading conditions:

- 1) internal pressure of 75.53 psi
- 2) inplane bending moment of 32,660 in-lb
- 3) out-of-plane bending moment of 32,660 in-lb
- 4) torsional moment of 32,660 in-lb

Figures 4-11 compare the smoothed NASTRAN stress curves as computed using Meshes A, B, and C with the experimental data points. The major and minor principal stress results are presented on alternating figures for each of the four loading conditions. Note that placing more strain gauges on the outer surface than on the inner surface of the pipe wall resulted in a greater number of experimental data points there. Also, for selected experiments, some gauge results were missing.

The following conclusions may be drawn from Figures 4-11:

1. The NASTRAN results using Meshes A and B (both ideal geometry) are in good overall agreement with the experimental results. Although

TABLE 4 - FLEXIBILITY FACTORS FOR MESH A

Moment Load	θ_a (rad)	θ_b	$\theta_{ab} = \theta_b - \theta_a$	θ_{nom}	k
In-plane	1.32×10^{-4}	11.08×10^{-4}	9.76×10^{-4}	1.57×10^{-4}	6.2
Out-of-plane	1.78×10^{-4}	7.19×10^{-4}	5.41×10^{-4}	1.57×10^{-4}	3.4
Torsion	1.32×10^{-4}	6.79×10^{-4}	5.47×10^{-4}	2.04×10^{-4}	2.7

flexibility factor = $k = \frac{\theta_{ab}}{\theta_{nom}}$

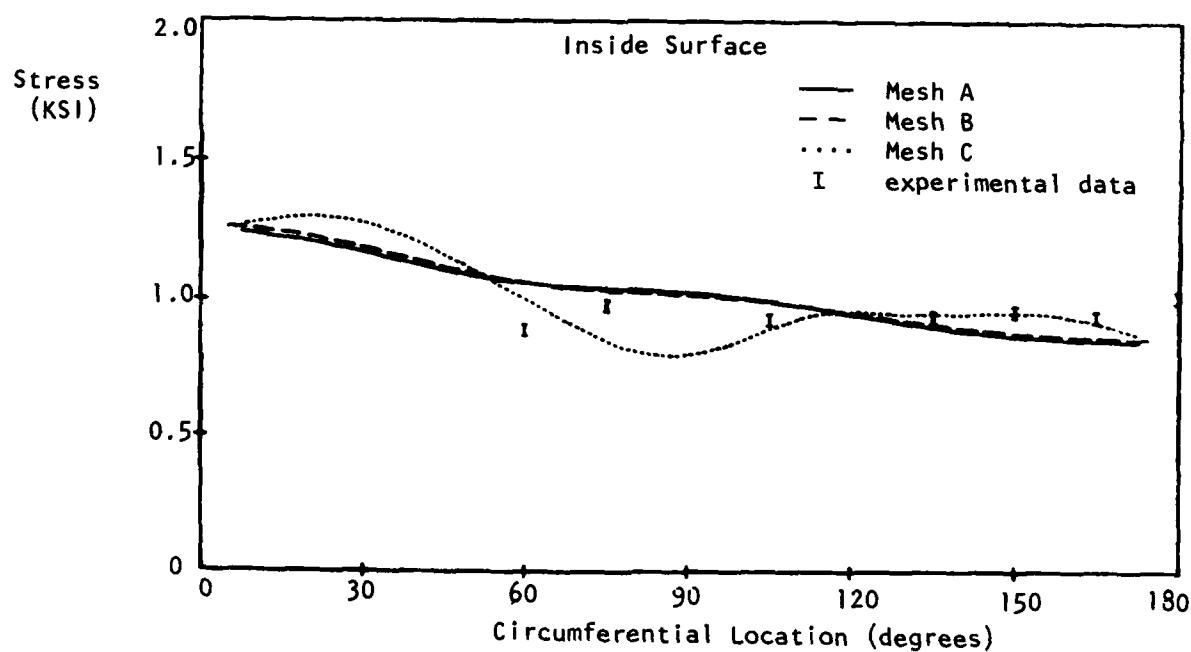
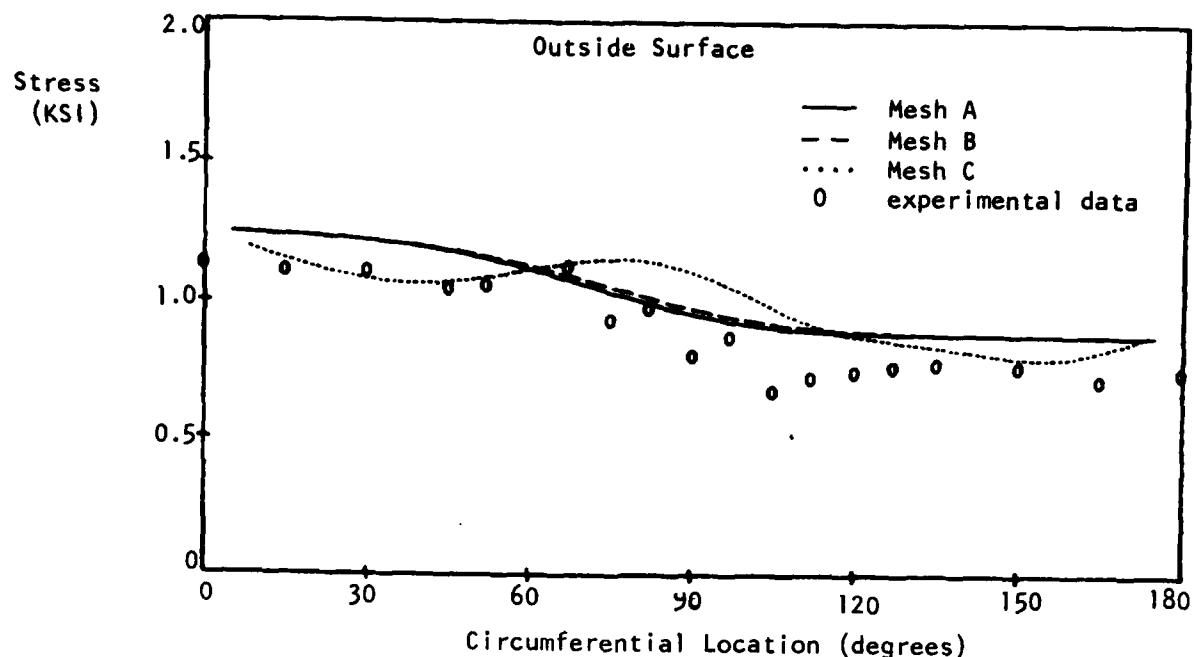


Figure 4 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Major Principal Stress, Pressure Load

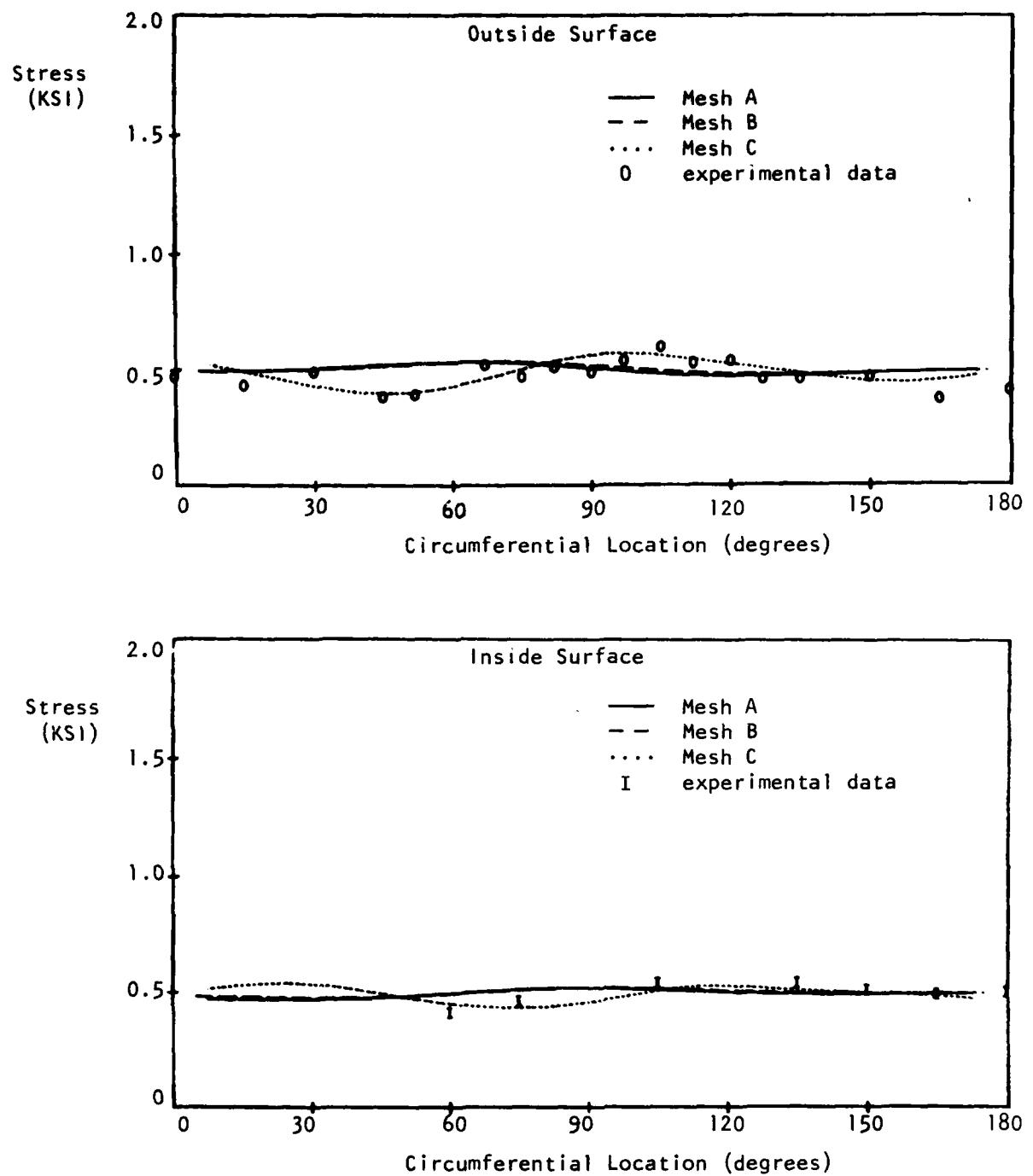


Figure 5 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Minor Principal Stress, Pressure Load

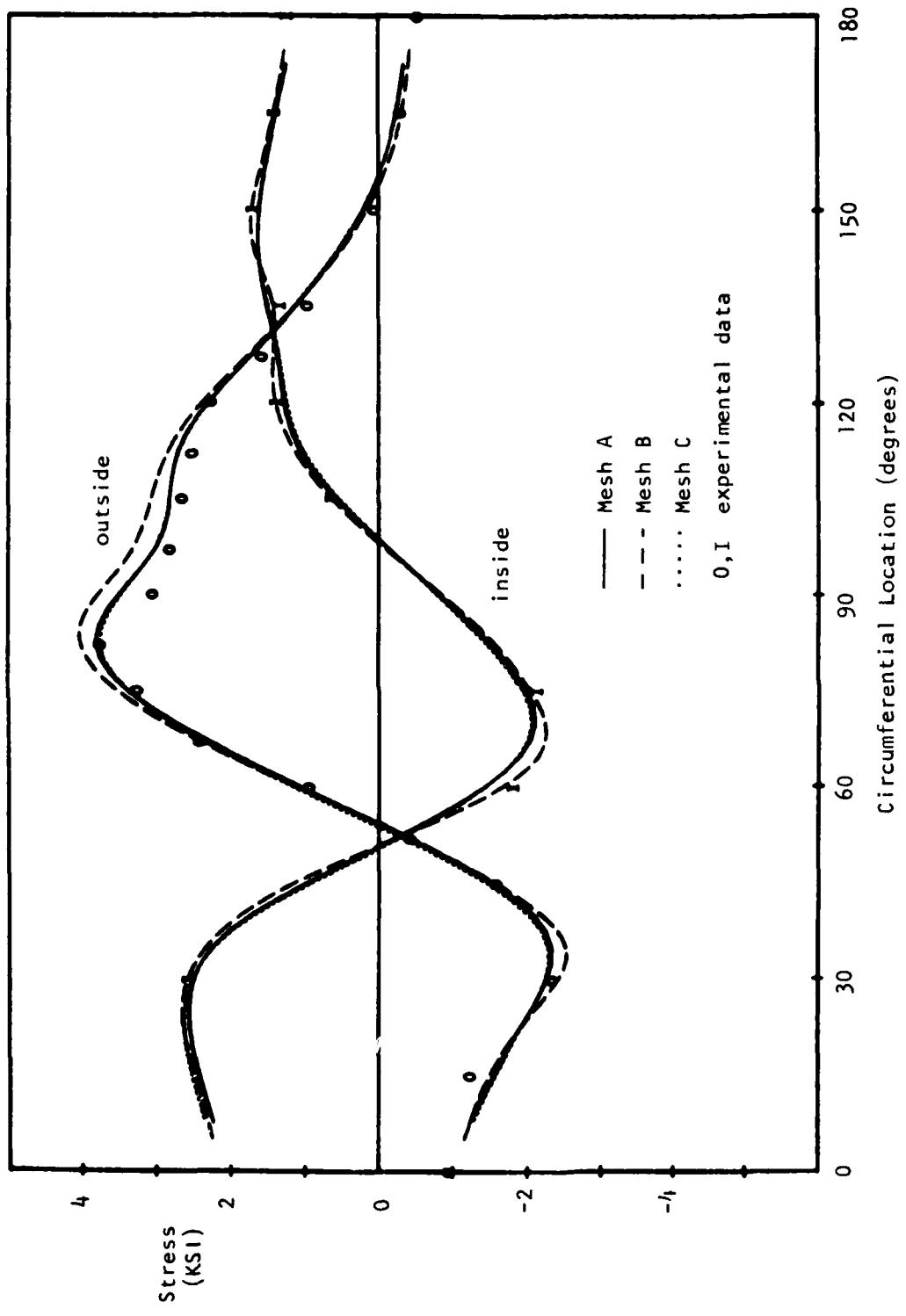


Figure 6 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Major Principal Stress, Inplane Moment Load

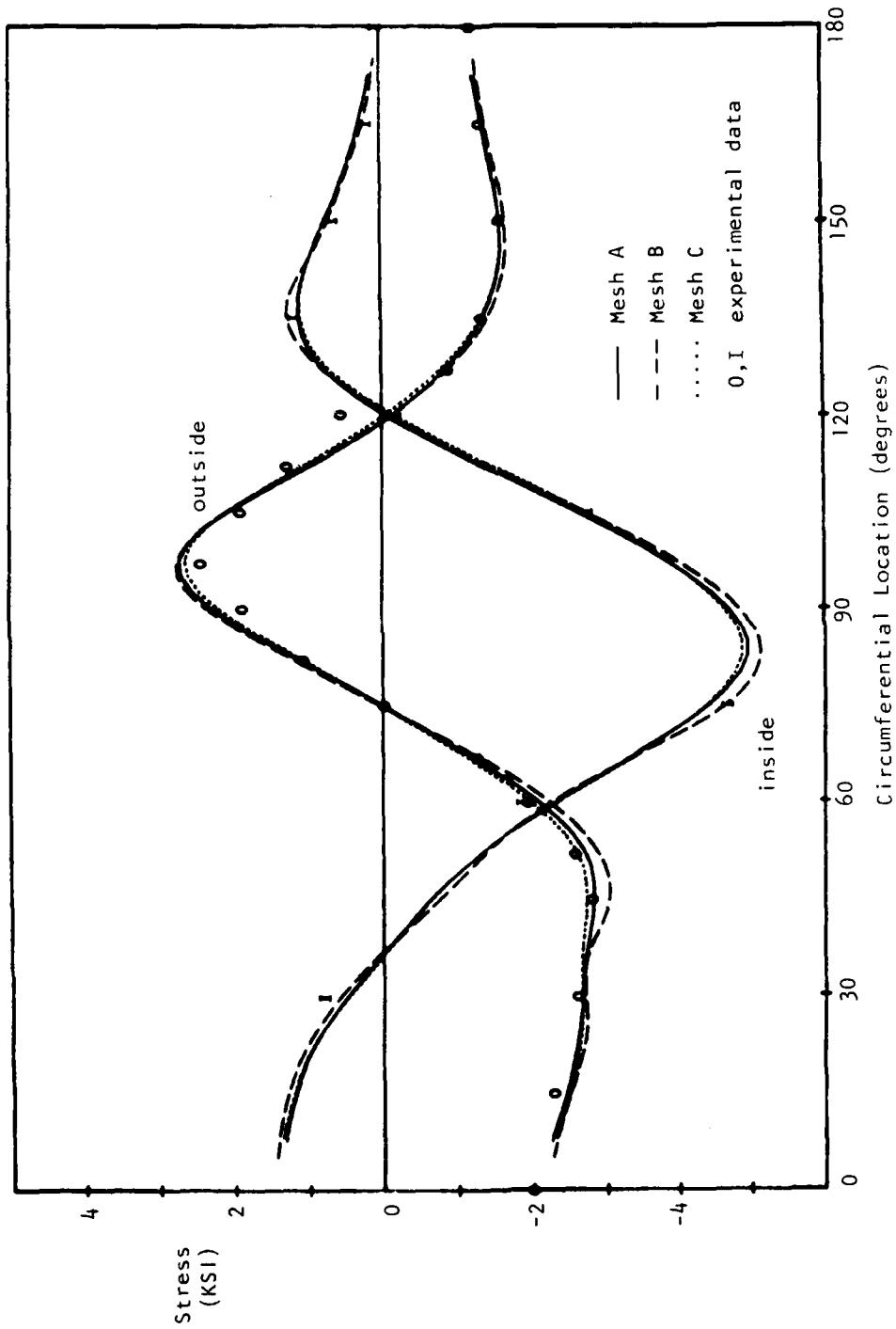


Figure 7 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Minor Principal Stress, Inplane Moment Load

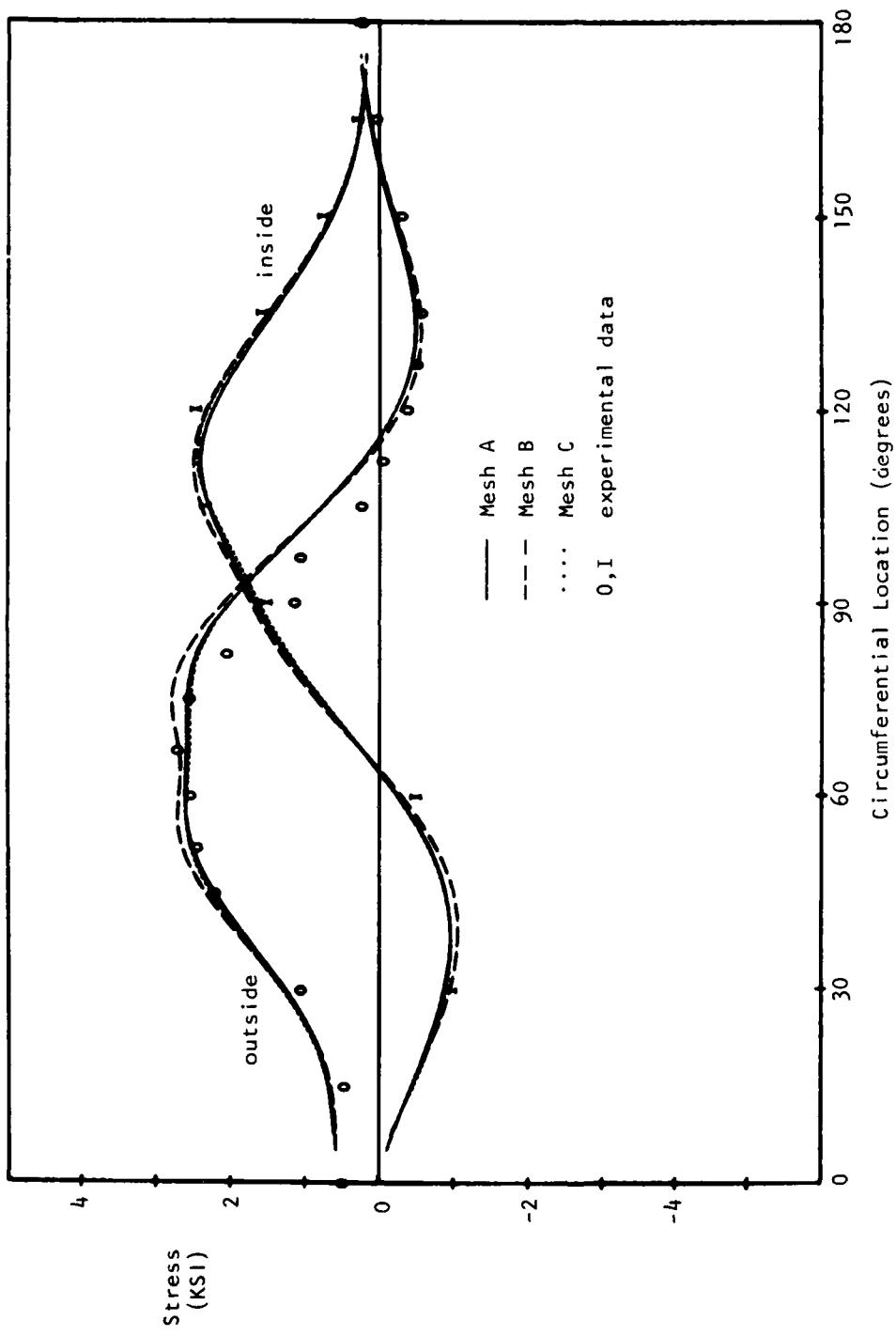


Figure 8 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Major Principal Stress, Out-of-Plane Moment Load

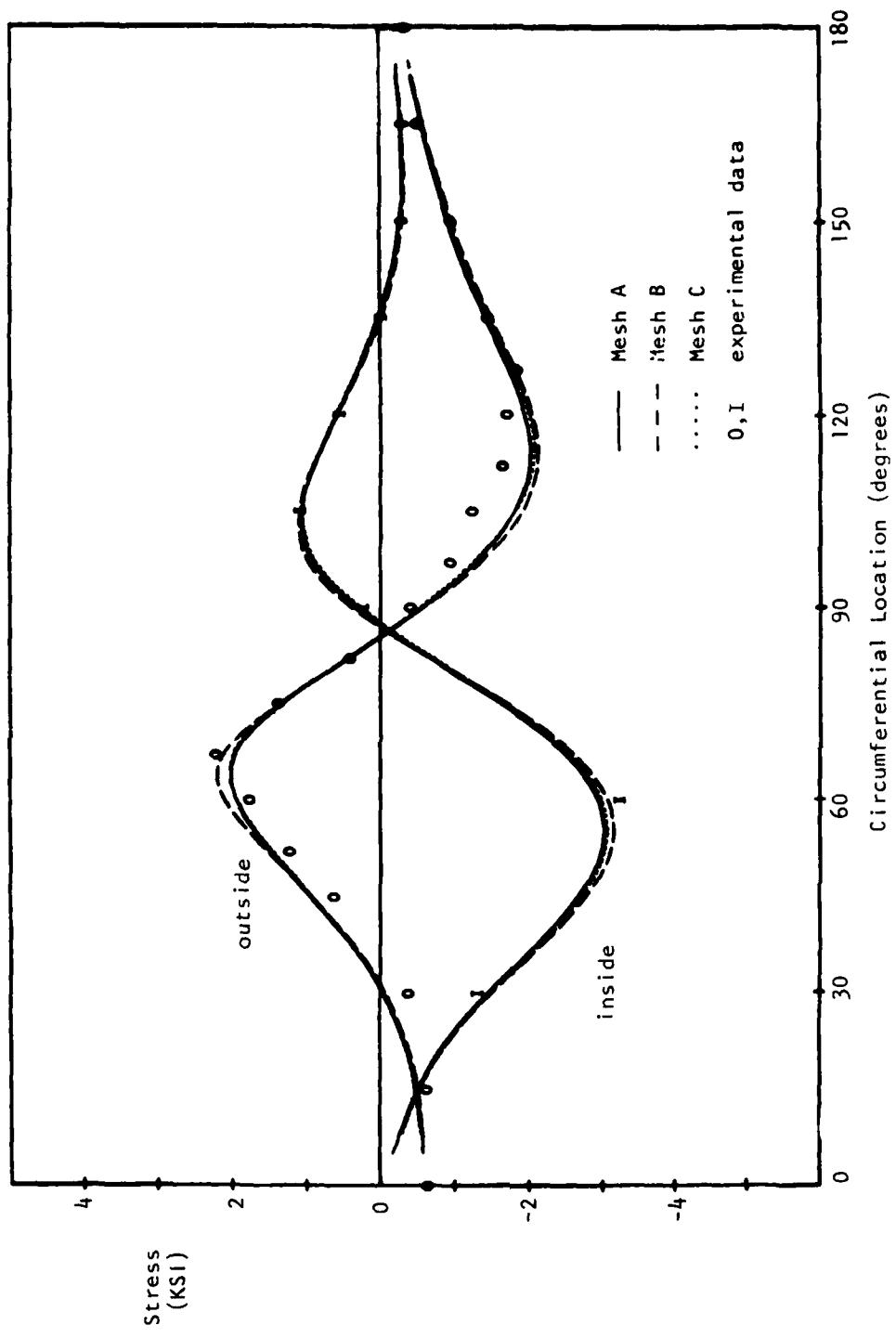


Figure 9 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Minor Principal Stress, Out-of-Plane Moment Load

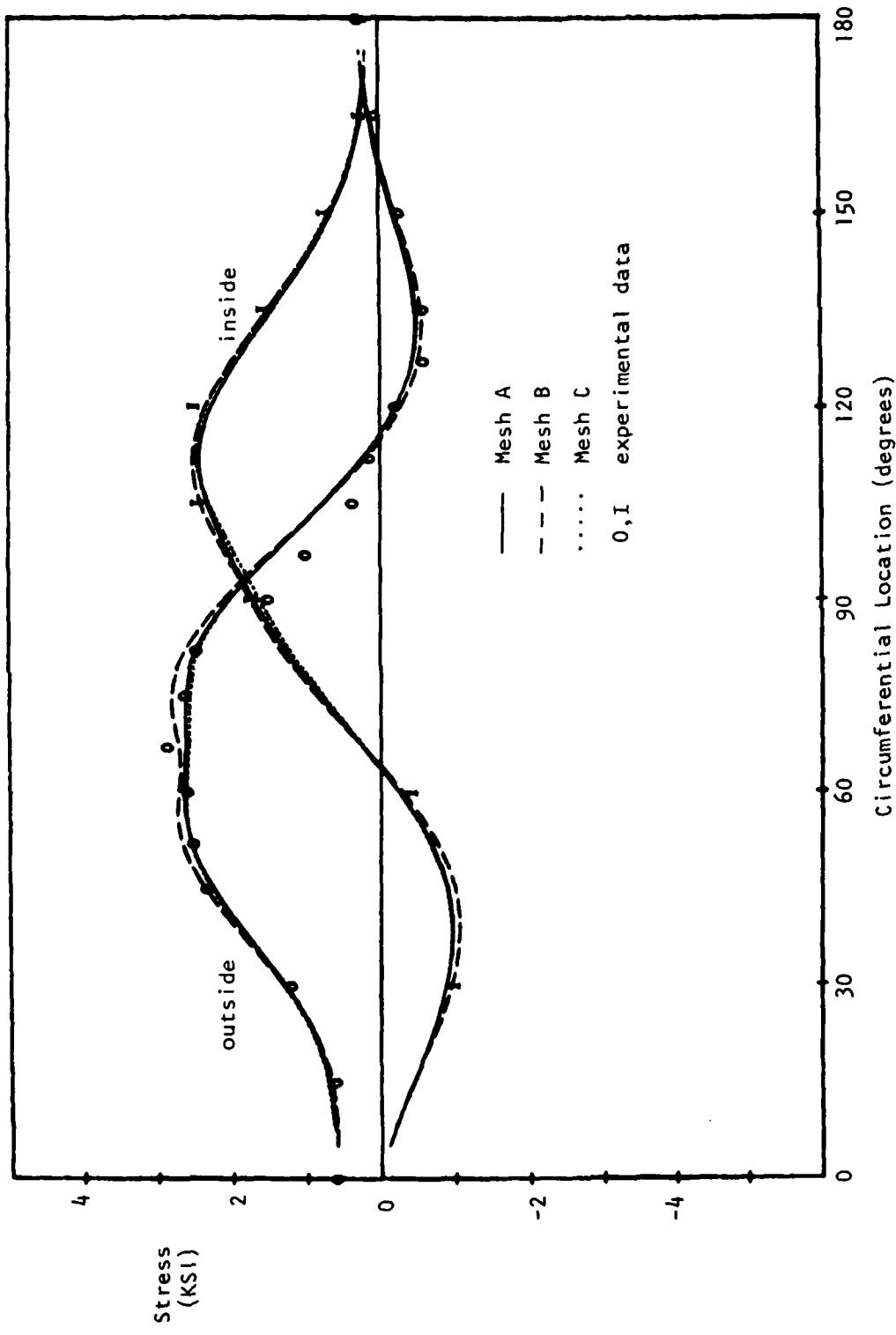


Figure 10 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Major Principal Stress, Torsion Moment Load

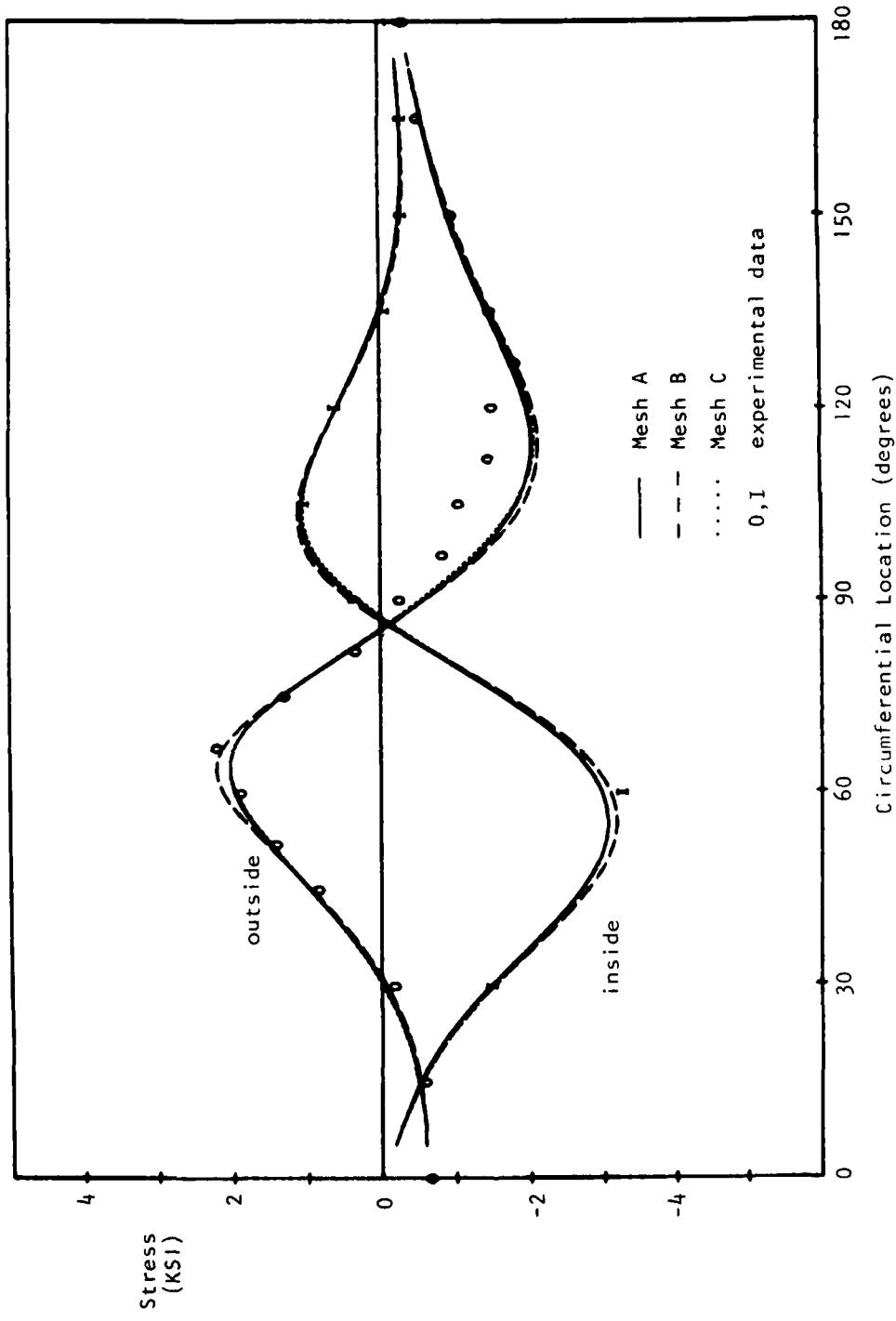


Figure 11 - Comparison of Computed and Experimental Stresses at Middle of Elbow - Minor Principal Stress, Torsion Moment Load

the coarser model (Mesh A) is non-conservative in that it underestimates (in absolute value) the stresses, its prediction of peak principal stresses is nevertheless excellent.

2. The Mesh C (actual geometry) results indicate that, except for internal pressure loading, the small variations in geometry shown in Tables 2 and 3 play an insignificant role in the stress computations. (The Oak Ridge researchers found in their more extensive experiments¹ that ovality in the pipe cross-section had a major influence on stresses only for pressure loading.)

3. When a large series of computer runs (e.g., a parameter study of pipe elbows) is contemplated, the gain in accuracy achieved with Mesh B (which has a fifty percent finer mesh spacing than Mesh A) would probably not be cost-effective. (The CDC 6400 computer charge at DTNSRDC was \$292 for Mesh B compared to \$99 for Mesh A.)

ACKNOWLEDGMENTS

The authors acknowledge with pleasure the fruitful discussions held with Mr. L. Kaldor and Dr. Y.P. Lu, both of the Engineering Analysis Branch (Code 2744), DTNSRDC.

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3. McKee, James M., "B-Spline Functions As a Solution to Some Knotty Geometric Modeling Problems," Proceedings of the Symposium on Computer Methods in Engineering, University of Southern California (Aug 1977).
4. McKee, J.M. and R.J. Kazden, "G-Prime B-Spline Manipulation Package--Basic Mathematical Subroutines," Report DTNSRDC 77-0036 (Apr 1977).
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APPENDIX A

Listing of Deck to Create UPDATE Program Library, Compile Source Code, and Catalog Executable Code for Elbow Data Generator

```
(JOB CARD)
(CHARGE CARD)
REQUEST,NEWPL,*PF.
UPDATE,F,C,N.
CATALOG,NEWPL,PFNAME1, ID=XXXX.
REQUEST,LGO,*PF.
FTN,OPT=1,R=3,PL=5000000,I=CDMPILE.
CATALOG,LGO,PFNAME2, ID=XXXX.
7/8/9 EOR **** SOURCE DECK FOR DATA GENERATOR FOLLOWS ****
*DECK ELB
      PROGRAM PIPELB(INPUT,DOUTPUT,TAPES=INPUT,TAPE6=DOUTPUT,TAPE8,TAPE9,
      - TAPE10,TAPE11,TAPE12,TAPE13,TAPE14,TAPE15,TAPE16,TAPE17,TAPE18,
      - TAPE19,TAPE20,TAPE21,TAPE22,TAPE23,TAPE24,TAPE25,TAPE26,TAPE27)
C
C      DATA GENERATOR FOR NASTRAN STRESS ANALYSIS OF A PIPE HAVING
C          THETA DEGREE ELBOW AND STRAIGHT SECTIONS
C      INPUT GENERATION INCLUDES FINITE ELEMENT PLATING (CQUAD2,GRID),
C          CONGRUENCY (CNGRNT) AND PRESSURE LOADING (PLOAD2) FOR ELEMENTS,
C          AND GRID POINT CONSTRAINTS (SPC)
C
C      MEL MARCUS,DTNSRDC 1843,JAN 1979
C
C      DIMENSION IDUM(8),ICNGR(35,24)
C      INTEGER ASET(24)
C      COMMON/A/THETA,NPH1,DPH,RPIPS,PIDS,LOADID,PLOAD
C      COMMON/B/NX,NY,TABX(9),TABY(7),TABF(9,7,2)
C      INTEGER          EID,PIDS,PID,SID,G(4)
C      INTEGER CPC,CDC
C      DATA PI,/3.141592654/
C
C      1 FORMAT (1H1)
C      3 FORMAT (10F8.3)
C      4 FORMAT (24I3)
C      8 FORMAT (8A10)
C      9 FORMAT (BHCBAR    ,4I8,3F8.1,18)
C     10 FORMAT (BHCNGRNT   ,2I8)
C     11 FORMAT (BHCQUAD2   ,6I8)
C     12 FORMAT (BHPGRID    ,2I8,F8.4,F8.3,F8.4,2I8)
C     15 FORMAT (BHPLOAD2   ,18,F8.3,18)
C     16 FORMAT (BHPQUAD2   ,2I8,F8.3)
C     17 FORMAT (BHSPEC    ,3I8)
C     26 FORMAT (BHSET 1 = ,8(I6,2H, )/(BX, B(I6,2H, )))
C     27 FORMAT (8X,16)
C     28 FORMAT (BHFORCE   ,3I8,F8.4,3F8.0)
C
C
C      PRESENTED BELOW ARE THE 4 READ ITEMS WHICH OCCUR IN PIPELB
C      ALSO INDICATED ARE THE 4 READ ITEMS WHICH FOLLOW
C          IN 2 CALLS TO SUBROUTINE STRATE
C
C      PHI=PORTION OF PIPE CIRCUMFERENCE MODELED, DEGREES
C      THETA=PORTION OF ELBOW ARC MODELED,DEGREES
C
C      PHI=180.
C      READ (5,3) THETA
C      WRITE (6,3) THETA
C
C      NPHI=NUMBER OF ELEMENTS IN PHI DIRECTION
C      NTHETA=NUMBER OF ELEMENTS IN THETA DIRECTION (COORD SYSTEM CPC)
C
C      READ (5,4) NPHI,NTHETA
```

```

      WRITE (6,4) NPHI,NTHETA
C   RBEND=BEND RADIUS MEASURED TO PIPE CENTERLINE
C   RPIPS,PIDS=NOMINAL VALUES OF PIPE RADIUS ,THICKNESS (PROPERTY ID)
C
C   PIDS=200
READ (5,3) RBEND,RPIPS
WRITE (6,3) RBEND,RPIPS
C
C   THIS ITEM CONTAINS A SINGLE READ (BLANK CARD)
C   OR MULTIPLE (3+NF*NY) READS
C   DEPENDING ON WHETHER NF=0 (IDEAL ELBOW)
C   OR NF=2 (VARIABLE RADIUS AND THICKNESS)
C
C   NX,NY=NUMBERS OF PHI,THETA-DIRECTION VALUES (TABX,TABY)
C   AT WHICH TABULATED VALUES OF
C   RADIUS AND THICKNESS (NF=2) ARE SPECIFIED FOR ELBOW
C
C   IF NF=0, THEN NOMINAL VALUES OF OF PIPE RADIUS
C   AND THICKNESS ARE USED THROUGHOUT
C   OTHERWISE, VARIABLE RADIUS AND THICKNESS VALUES ARE COMPUTED
C   FOR THETA-DIR VALUES BETWEEN TABY(1) AND TABY(NY) DEGREES
C   WITH NOMINAL VALUES USED ELSEWHERE
C
READ (5,4) NX,NY,NF
WRITE (6,4) NX,NY,NF
IF (NF.EQ.0) GO TO 45
READ (5,3) (TABX(I),I=1,NX)
WRITE (6,3) (TABX(I),I=1,NX)
READ (5,3) (TABY(I),I=1,NY)
WRITE (6,3) (TABY(I),I=1,NY)
DO 40 K=1,NF
DO 40 J=1,NY
READ (5,3) (TABF(I,J,K),I=1,NX)
WRITE (6,3) (TABF(I,J,K),I=1,NX)
40 CONTINUE
45 CONTINUE
C
C   THE 2 ITEMS READ NEXT ARE TRIGGERED BY "CALL STRATE(1)"
C   THE ITEMS TO BE READ ARE DESCRIBED ATOP SUBROUTINE STRATE
C
C   THE LAST 2 ITEMS READ ARE TRIGGERED BY "CALL STRATE(2)"
C   THE ITEMS TO BE READ ARE DESCRIBED ATOP SUBROUTINE STRATE
C
C
CPC=1
CDC=1
MID=45
LOADID=21
PLOAD=-1.
C
DPH=PHI/NPHI
DTH=THETA/NTHETA
NPHI=NPHI+1
NTH1=NTHETA+1
IHTH=NTH1/2
C
C   END CAP LOAD DUE TO UNIT INTERNAL PRESSURE - 27
C
CAPLD=.5*NPHI*RPIPS*RPIPS*SIN(DPH *PI/180.)
WRITE (27,28) LOADID,200500,3,CAPLD,0.,0.,-1.
C

```

```

C
C      GENERATE FE PLATING FOR STRAIGHT SECTION (TOP)
C      CHECK SUBROUTINE STRATE FOR INPUT TO BE READ IN
C      CALL STRATE (1)
C
C      GENERATE FE PLATING FOR ELBOW
C
C      TH=0.
C      IBASE=500000
C
C      DO 200 I=1,NTH1
C      PID=PIDS
C      RPIPE=RPIPS
C      ITH=TH+.5
C      INEXT=TH+DTH+.5
C      IMOVE=1000*(INEXT-ITH)
C      PH=0.
C      ID=IBASE
C
C      DEFINE MYTHICAL CENTER POINTS ALONG ELBOW
C
C      NBARS=0
C      IDCEN=ID+500
C
C      DO 150 J=1,NPH1
C
C      SPOKES (CBAR - 9) CONVERGE TO MYTHICAL CENTERS AT ELBOW ENDS
C
C      IF (I.NE.1.AND.I.NE.NTH1) GO TO 50
C      NBARS=NBARS+1
C     >IDBAR=IDCEN+NBARS
C      IF (J.EQ.1.OR.J.EQ.NPH1) GO TO 52
C      WRITE (9,9)IDBAR,PIDS+2,ID, IDCEN,0.,1.,0.,1
C      GO TO 50
C      52 WRITE (9,9)IDBAR,PIDS+1, ID, IDCEN,0.,1.,0.,1
C      50 CONTINUE
C
C      IPH=PH+.5
C      INEXT=PH+DPH+.5
C      JMOVE=INEXT-IPH
C
C      POSSIBLY INTERPOLATE FOR PIPE RADIUS
C
C      IF (NF.EQ.0) GO TO 60
C      IF (TH.GT.TABY(NY)) GO TO 62
C      CALL FIND (PH,TH,1,THICK)
C      CALL FIND (PH,TH,2,OD)
C      RPIPE=.5*(OD-THICK)
C      IREG=NTH1
C      GO TO 64
C      60 IREG=1
C      GO TO 64
C      62 IREG=I
C      64 IREG1=IREG+1
C
C      GRID FOR ELBOW - 13
C

```

```

C      ELBOW MODELED IN CYLINDRICAL R,T,Z COORD SYSTEM CPC
C      IN WHICH T IS PORTION OF THETA
C
C      ANG=PH+PI/180.
C      R=RBEND-RPIPE*COS(ANG)
C      Z=RPIPE*SIN(ANG)
C      WRITE (13,12) ID,CPC,R,TH,Z,CDC
C      IF (J.EQ. NPH1) GO TO 20
C      IF (I.EQ. NTH1) GO TO 115
C
C      ICEN=TH+.5*DTH+.5
C      JCEN=PH+.5*DPH+.5
C      EID=1000*ICEN+JCEN+500000
C      IF (I.EQ.IHTH) ASET(J)=EID
C
C      ASSIGNING CONGRUENCY
C
C      ICNGR(I,J)=EID
C
C      POSSIBLY INTERPOLATE FOR PIPE THICKNESS
C      IF SO , GENERATE PROPERTY CARD - 18
C
C      IF (NY.EQ.0) GO TO 80
C      IF (IH.GT.TABY(NY)) GO TO 80
C      PID=EID
C      PC=PH+.5*DPH
C      TC=TH+.5*DTH
C      CALL FIND (PC,TC,1,THICK)
C      WRITE (16,16) PID,MID,THICK
80 CONTINUE
C
C      CQUAD2 FOR ELBOW - 11
C
C      G(1)=ID
C      G(2)=G(1)+IMOVE
C      G(3)=G(2)+JMOVE
C      G(4)=G(3)-IMOVE
C      WRITE (11,11) EID,PID,(G(L),L=1,4)
C
C      PLOAD2 FOR QUADS - 15
C
C      WRITE (15,15) LOADID,PLOAD,EID
115 IF (J.NE.1) GO TO 100
C
C      SPC FOR ELBOW - 18,21
C          SYM B.C. AT PHI=0,180 - 18
C          ANTI- SYM B.C. AT PHI=0,180 - 21
C
20 SID=71
L=345
WRITE (18,17) SID,ID,L
SID=72
L=126
WRITE (21,17) SID,ID,L
C
100 ID=ID+JMOVE
PH=PH+DPH
C
C      150 CONTINUE
C
C      IBASE=IBASE+IMOVE

```

```

TH = TH +DTH
200 CONTINUE
C
C      CNGRNT (THETA DIRECTION ONLY) FOR ELBOW - 10
C
C      IF (IREG .GE. NTHETA) GO TO 210
DO 205 J=1,NPHI
DO 205 I=IREG1,NTHETA
205 WRITE (10,10) ICNGR(IREG,J),ICNGR(I,J)
210 CONTINUE
C
C      SOLUTION SET FOR CASE CONTROL - 26
C
C      WRITE (26,26) (ASET(J),J=1,NPHI)
WRITE (26,27) 999999
C
C      GENERATE FE PLATING FOR STRAIGHT SECTION (BOTTOM)
C      CHECK SUBROUTINE STRATE FOR INPUT TO BE READ IN
CALL STRATE (2)
C
C
C      WRITE (6,1)
DO 1000 I=9,27
REWIND I
910 READ (I,8) (IDUM(K),K=1,8)
IF (EOF(I).NE.0) GO TO 920
WRITE(8,8) (IDUM(K),K=1,8)
GO TO 910
920 REWIND I
1000 CONTINUE
REWIND 8
C
C      STOP
END
SUBROUTINE STRATE (IFLAG)
C
C      GENERATE FE PLATING FOR STRAIGHT SECTION
C      IFLAG=1,2 INDICATES PORTION ABOVE,BELOW ELBOW
C
DIMENSION ZS(25),IZDZCH(6),KOUNT( 5 ),IJCNGR(5,500)
COMMON/A/THETA,NPH1,DPH,RPIPS,PIDS,LOADID,PLOAD
INTEGER CPS,CDS,EID,PIDS,PID,SID,G(4)
C
2 FORMAT (I8,9F8.2/(10F8.2))
4 FORMAT (24I3)
10 FORMAT (8HCNGRNT ,2I8)
11 FORMAT (8HCQUAD2 ,6I8)
12 FORMAT (8HGRID ,2I8,F8.4,F8.3,F8.4,2I8)
15 FORMAT (8HUPLOAD2 ,I8,F8.3,I8)
17 FORMAT (8HSPC ,3I8)
25 FORMAT (8HCGRID1 ,3I8)
C
C      STRAIGHT SECTION MODELED IN CYLINDRICAL R,T,Z COORD SYSTEM CPS
C      IN WHICH Z IS DISTANCE ALONG STRAIGHT EDGE
C      ( Z=0 AT POINTS OF CURVATURE/TANGENCY )
C
C

```

```

C      NZS1=NUMBER OF GRID POINTS IN Z DIRECTION
C      ZS(I)=Z-COORDS OF THE NZS1 PTS IN COORD SYSTEM CPS
C
C      FOR IFLAG=1, VALUES BEGIN AT Z=-L1 AND END AT Z=0
C      FOR IFLAG=2, VALUES BEGIN AT Z=0 AND END AT Z=L2
C          WHERE L1,L2 ARE PIPE LENGTHS ABOVE,BELOW ELBOW
C
C      READ (5,2) NZS1,(ZS(I),I=1,NZS1)
C      WRITE (6,2) NZS1,(ZS(I),I=1,NZS1)
C
C      NDZCHS=NUMBER OF CHANGES IN DZ=ZS(I+1)-ZS(I)
C      IZDZCH(K)=VALUES OF I , I=1 TO NZS1, AT WHICH DZ CHANGES
C          (CONVENTION IS TO SPECIFY I=1 AS A CHANGE)
C
C      READ (5,4) NDZCHS,(IZDZCH(K),K=1,NDZCHS)
C      WRITE (6,4) NDZCHS,(IZDZCH(K),K=1,NDZCHS)
C
C
C      SET UP CONGRUENCY SETS
C
C      IBOOM=0
C      NSETS= NDZCHS
C      DO 650 I=1,NSETS
C      650 KOUNT(I)=0
C
C      IF (IFLAG.EQ.2) GO TO 20
C      CPS=3
C      CDS=3
C      NTPGRD=12
C      NTPSYM=17
C      NTPAS=20
C      ILIM=NZS1-1
C      IBASE=(500-10*ILIM)*1000
C      IRIGID=IBASE
C      GO TO 30
C      20 CPS=2
C      CDS=2
C      NTPGRD=14
C      NTPSYM=19
C      NTPAS=22
C      ILIM=NZS1
C      IBASE=(500+THETA)*1000
C      30 RPIPE=RPIPS
C      PID=PIIDS
C
C      DO 400 I=1,ILIM
C      IMOVE=10000
C      PH=0.
C      ID=IBASE
C
C      DO 350 J=1,NPH1
C      IPH=PH+.5
C      INEXT=PH+DPH+.5
C      JMOVE=INEXT-IPH
C
C      RIGID ELEMENTS AT FREE END - 25
C
C      IF (I.NE.1.OR.IFLAG.NE.1) GO TO 27
C      WRITE (25,25) J+1,200500,IRIGID

```

```

IRIGID=IRIGID+JMOVE
27 CONTINUE
C
C
C     GRID FOR STRAIGHT SECTION - NTPGRD
C
IF (IFLAG.EQ.2.AND.I.EQ.1) GO TO 202
NT=NTPGRD
WRITE (NT,12) ID,CPS,RPIPE,PH,?S(I),CDS
202 IF (J.EQ. NPH1) GO TO 220
IF (IFLAG.EQ.2.AND.I.EQ.ILIM) GO TO 215
C
EID=ID
IF (IFLAG.EQ.1.AND.I.EQ.ILIM) GO TO 204
IF (IFLAG.EQ.2.AND.I.EQ.1) GO TO 204
C
C     TESTING FOR AND ASSIGNING CONGRUENCY
C
IBOOM=IBOOM+1
IZDZCH(NDZCHS+1)=NZS1
DO 700 K=1,NDZCHS
NSET=0
IZ1=IZDZCH(K )-1
IZ2=IZDZCH(K+1)-1
IF (I.GT.IZ1.AND.I.LE.IZ2) NSET=K
IF (NSET.EQ.0) GO TO 700
IF (IBOOM.EQ.1) NSET1=NSET
NSETS=NSET
KOUNT(NSET)=KOUNT(NSET)+1
KNT=KOUNT(NSET)
IJLNGR(NSET,KNT) =EID
700 CONTINUE
C
C     CQUAD2 FOR STRAIGHT SECTION - 11
C
204 G(1)=ID
G(2)=G(1)+IMOVE
G(3)=G(2)+JMOVE
G(4)=G(3)-IMOVE
WRITE (11,11) EID,PID,(G(L),L=1,4)
C
C     PLOAD2 FOR QUADS - 15
C
WRITE (15,15) LOADID,PLOAD,EID
IF (IFLAG.EQ.1.AND.I.EQ.1) GO TO 300
215 IF (J.EQ.1) GO TO 220
IF (IFLAG.EQ.2.AND.I.EQ.ILIM) GO TO 225
GO TO 300
C
C     SPC FOR STRAIGHT SECTION - NTPSYM,NTPAS,23,24
C     SYM B.C. AT PHI=0,180 - NTPSYM
C     ANTI- SYM B.C. AT PHI=0,180 - NTPAS
C     ELIM ZERO DOF AT PHI=0,180 - 23
C     CONSTRAIN FIXED END - 24
C
220 IF (I.EQ.1) GO TO 300
SID=71
L=246
NT=NTPSYM
WRITE (NT,17) SID,ID,L
SID=72
L=135
NT=NTPAS

```

```

        WRITE (17) SID, ID, L
        SID=80
        L=4
        WRITE (17) SID, ID, L
        IF (IFLAG.EQ.2.AND.I.EQ.ILIM) GO TO 225
        GO TO 300
225 SID=85
        L=123456
        WRITE (17) SID, ID, L
C
300 ID=ID+JMOVE
        PH=PH+DPH
C
C
350 CONTINUE
        IBASE=IBASE+IMOVE
C
C
400 CONTINUE
C
C
C     CNGRNT (BOTH DIRECTIONS) FOR STRAIGHT SECTION - 10
C
        DO 405 K=NSET1,NSETS
        KNT=KOUNT(K)
        DO 405 L=2,KNT
        405 WRITE (10,10) IJCNGR(K,1),IJCNGR(K,L)
C
C
        RETURN
        END
        SUBROUTINE FIND (X,Y,K,FXY)
C
C     INTERPOLATE FOR FUNCTIONAL VALUES WHICH ARE
C     TABULATED FOR BOTH X AND Y TABULATED VALUES
C
C     K INDICATES FUNCTION BEING CONSIDERED
C
        DIMENSION FX(7)
        COMMON/B/NX,NY,TABX(9),TABY(7),TABF(9,7,2)
C
        DO 10 J=2,NY
        IF (TABY(J).GT.Y) GO TO 15
10 CONTINUE
        J2=NY
        GO TO 20
15 J2=J
20 J1=J2-1
C
        DO 30 I=2,NX
        IF (TABX(I).GT.X) GO TO 35
30 CONTINUE
        I2=NX
        GO TO 40
35 I2=I
40 I1=I2-1
C
        XRAT=(X-TABX(I1))/(TABX(I2)-TABX(I1))
        DO 50 J=J1,J2
50 FX(J)=TABF(I1,J,K)+XRAT*(TABF(I2,J,K)-TABF(I1,J,K))
C
        YRAT=(Y-TABY(J1))/(TABY(J2)-TABY(J1))
        FXY=FX(J1)+YRAT*(FX(J2)-FX(J1))
C
        RETURN
        END
6/7/8/9 EOF

```

APPENDIX B
Listing of Deck to Execute Elbow Data Generator
and Create NASTRAN Input Data File for Mesh A

```
(JOB CARD)
(CHARGE CARD)
ATTACH,PIPELB,PFNAME2,ID=XXXX.
PIPELB.
REQUEST,NEWPL,+PF.
UPDATE,F,C,N,D.
CATALOG,NEWPL,PFNAME3,ID=XXXX.
COPYSBF,COMPILE.
7/8/9 EOR **** INPUT DATA (MESH A) FOR DATA GENERATOR FOLLOWS ****
90.
 12 17
15.0   5.163
(BLANK CARD)
 12 -21.   -18.5   -16.5   -14.5   -12.5   -10.5   -8.5   -6.5   -4.5
-2.5    -1.     0.
 4 1 2 10 11
 12 0.     1.     2.5     4.5     6.5     8.5     10.5    12.5    14.5
16.5   18.5   20.5
 3 1 2 3
7/8/9 EOR **** INPUT DECK TO UPDATE FOLLOWS ****
*DECK DATA
NASTRAN CONFIG=6,FILES=(PLT2,NPTP,OPTP,INPT)
ID PIPE,ELBOW
APP DISP
SOL 1,0
TIME 25
$SEQUENCE YES
$GRID=525
$CONFIG=6
CEND
TITLE =STRESS ANALYSIS OF ELBOW ME-1 (ORNL-TM-4834)
MAXLINES=500000
*READ TAPE26
DISP=ALL
STRESS(PRINT,PUNCH)=1
SPCFORCE=ALL
$
$      SUBCASES HAVING SAME B.C. ARE GROUPED TOGETHER
$      TO AVOID UNNECESSARY MATRIX DECOMPOSITIONS
$
SUBCASE 1
  SUBTITLE=UNIT PRESSURE LOAD
  LABEL=SYM B.C.
  LOAD=21
  SPC=91
  OLOAD=ALL
  STRESS=1
SUBCASE 2
  SUBTITLE=UNIT IN-PLANE (Z) MOMENT
  LABEL=SYM B.C.
  LOAD=22
  SPC=91
  OLOAD=ALL
  STRESS=1
SUBCASE 3
  SUBTITLE=UNIT OUT-OF-PLANE (X) MOMENT
  LABEL=ANTI-SYM B.C.
  LOAD=23
  SPC=92
  OLOAD=ALL
  STRESS=1
SUBCASE 4
  SUBTITLE=UNIT TORSIONAL (Y) MOMENT
```

```

LABEL=ANTI-SYM S.C.
LOAD=24
SPC=92
OLOAD=ALL
STRESS=1
SUBCOM 21
SUBTITLE=PRESSURE LOAD OF 75.53 PSI
SUBSEQ=75.53,0.,0.,0.
SUBCOM 22
SUBTITLE=IN-PLANE MOMENT OF 32660 IN-LB
SUBSEQ=0.,-32660.,0.,0.
SUBCOM 23
SUBTITLE=OUT-OF-PLANE MOMENT OF 32660 IN-LB
SUBSEQ=0.,0.,32660.,0.
SUBCOM 24
SUBTITLE= TORSIONAL MOMENT OF 32660 IN-LB
SUBSEQ=0.,0.,0.,32660.

$  

$  

$      STRUCTURE     ...PIPE (RPIPE=5.163) CONSISTS OF  

$          90 DEGREE ELBOW (RBEND=15.0)  

$          ADJOINED BY STRAIGHT SECTIONS  

$  

$      SYMMETRY      ...IMPOSED AT PIPE HALF-CIRCUM (PHI=0,180)  

$  

$      COORD SYSTEMS...(ELBOW) R=RBEND-RPIPE*COS(PHI)  

$          T=THETA, (THETA=0,90 AT P.C.,P.T.)  

$          Z=RPIPE*SIN(PHI)  

$  

$      COORD SYSTEMS...(STRAIGHT SEC) R=RPIPE  

$          T=PHI  

$          (TOP) Z=DISTANCE FROM P.C.  

$          (BOTTOM) Z=DISTANCE FROM P.T.  

$  

$      NODAL VALUES ... (ELBOW)      ID=1000*(500+ITH)+IPH  

$          WHERE ITH ARE ROUNDED NODAL VALUES OF THETA  

$          IPH ARE ROUNDED NODAL VALUES OF PHI  

$  

$          (STRAIGHT SEC)  

$          (TOP) ID=1000*(500-10*(J-I))+IPH  

$              I=0,1,2,...,J-1  

$          (BOTCM) ID=1000*(590+10*I)+IPH  

$              I=1,2,...,K  

$          WHERE J IS NO. OF Z-INTERVALS SUBDIVIDING TOP SEC  

$          K IS NO. OF Z-INTERVALS SUBDIVIDING BOT SEC  

$  

$  

$  

$      BEGIN BULK  

$  

$          SPOKES AT ELBOW ENDS CONVERGE TO MYTHICAL CENTER POINTS  

$  

*READ TAPE9
$  

$          ELEMENT CONGRUENCY...(ELBOW)      THETA DIRECTION ONLY  

$          (STRAIGHT SEC) BOTH DIRECTIONS  

$  

*READ TAPE10
$  

$          ELBOW DEFINED IN COORD SYSTEM 1  

$          STRAIGHT BOTTOM DEFINED IN COORD SYSTEM 2  

$          STRAIGHT TOP    DEFINED IN COORD SYSTEM 3  

$          ORNL CARTESIAN SYSTEM IS NO. 4

```

```

$ CORD2C 1 0 0. 0. 0. 0. 0. 1. +COR1
$ +COR1 1. 0. 0. 0. 0. -1. 15. 0. +COR2
$ CORD2C 2 0 0. 15. 0. 0. 15. 1. 0. +COR3
$ +COR2 0. 14. 0. 0. 0. 0. 0. -1. +COR4
$ CORD2C 3 0 0. 15. 0. 0. 15. 1. 0. +COR3
$ +COR3 14. 0. 0. 0. 0. 0. 0. -1. +COR4
$ CORD2R 4 0 0. 0. 0. 0. 0. 0. +COR4
$ +COR4 1. 0. 0. 0. 0. 0. 0. -1. +COR1

$ FINITE ELEMENT PLATING
$ *READ TAPE11
$ RIGID CONNECTION FOR FREE (LOADED) END OF PIPE
$ CRIGD1 1 200500 100500
$ *READ TAPE25
$ END CAP LOAD DUE TO UNIT INTERNAL PRESSURE
$ *READ TAPE27
$ GRID POINTS
$ MYTHICAL CENTER POINT 1 UNIT BEYOND FREE END OF PIPE
$ GRID 100500 0 15.0 -22.0 0. 4
$ MYTHICAL CENTER POINT AT FREE END OF PIPE
$ GRID 200500 0 15.0 -21.0 0. 4
$ STRAIGHT SECTION ABOVE THETA=0
$ *READ TAPE12
$ MYTHICAL CENTER POINT AT THETA=0 END OF ELBOW
$ (EQUIV TO ORIGIN OF COORD SYS 3)
$ GRID 500500 0 15.0 0. 0. 4
$ ELBOW POINTS
$ *READ TAPE13
$ MYTHICAL CENTER POINT AT THETA=90 END OF ELBOW
$ (EQUIV TO ORIGIN OF COORD SYS 2)
$ GRID 590500 0 0. 15. 0. 4
$ STRAIGHT SECTION BELOW THETA=90
$ *READ TAPE14
$ MAT1 45 2.9+7 0.3 7.324-4 STEEL
$ BENDING MOMENTS APPLIED AT FREE END
$ MOMENT 22 200500 0 0.50 0. 0. 1.
$ MOMENT 23 200500 0 0.50 1. 0. 0.
$ MOMENT 24 200500 0 0.50 0. 1. 0.
$ PBAR 201 45 1.0-8 1.0-8 1.0-8 2.0-9

```

```
PBAR    202    45    2.0-6   2.0-9   2.0-9   4.0-9
$  
$      INTERNAL PRESSURE LOADING FOR PIPE
$  
*READ TAPE15
$  
PQUAD2  200    45    0.390
$  
$      SPC...(SID=71)      SYM B.C. AT MIDPLANE CUTTING PIPE CIRCUM
$  
SPC    71    200500  345
*READ TAPE17
SPC    71    500500  345
*READ TAPE18
SPC    71    590500  345
*READ TAPE19
$  
$      (SID=72)  ANTI-SYM B.C. AT MIDPLANE CUTTING PIPE CIRCUM
$  
SPC    72    200500  126
*READ TAPE20
SPC    72    500500  126
*READ TAPE21
SPC    72    590500  126
*READ TAPE22
$  
$      ELIMINATION OF ZERO STIFFNESS DOF
$  
*READ TAPE23
$  
$      CONSTRAIN FIXED END
$  
*READ TAPE24
$  
SPCADD 91    71    80    85
SPCADD 92    72    80    85
ENDDATA
6/7/8/9 EOF
```

APPENDIX C

Listing of Deck to Execute NASTRAN and Save Stresses at Middle of Elbow

```
(JOB CARD)
(CHARGE CARD)
LIMIT,13000.
MAP,OFF,
ATTACH,OLDPL,PFNAME3,1D=XXXX.
UPDATE,F,C=DATA,N,D.
ATTACH,NASTRAN.
REQUEST,PUN,*PF.
RFL,160000.
BEGIN,NASTRAN,NASTRAN,,DATA,,PUN.
CATALOG,PUN,PFNAME4,1D=XXXX.
7/8/9 EOR **** UPDATE CORRECTIONS (IF ANY) FOLLOW ****
6/7/8/9 EOF
```

APPENDIX D
Listing of Deck to Smooth Principal Stresses and
Create Solution File in PLOT QUICK Format

```
(JOB CARD)
(CHARGE CARD)
ATTACH,TAPE9,PFNAME4,ID=XXXX.
REQUEST,TAPE10,*PF.
ATTACH,PROD,461PRODUCTS,ID=CSYS.
ATTACH,BSPLNLB,1D=CAMK.
LIBRARY,PROD,BSPLNLB.
LOADLDR.
FTN.
LOADLDR.
LGO.
CATALOG,TAPE10,PFNAME5,ID=XXXX.
7/8/9 EOR **** SOURCE DECK FOLLOWS ****
      PROGRAM PREPLT(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE9,TAPE10)
C
C
C
C      THIS PROGRAM READS (TAPE9) NASTRAN-GENERATED ELBOW STRESS OUTPUT,
C      SELECTS FROM IT A SOLUTION SUBSET,
C      SMOOTH THIS SOLUTION SET,
C      AND THEN SCALES + SAVES THE ORIGINAL AND SMOOTHED SOLUTION SETS,
C      EACH IN A PLOTQUICK (INTERACTIVE PLOTTING) FORMAT ON TAPE10
C
C
C      CARD INPUT CONSISTS OF NPTS,THE NO. OF ELMTS IN CIRCUMFER DIREC,
C      FOLLOWED BY A SHORT AND LONG NAME, TITS AND TITL, RESPECTIVELY,
C      FOR EACH OF THE 34 CURVES WHICH GIVE,
C      IN AN ALTERNATING (UNSMOOTHED AND SMOOTHED) PATTERN,
C      THE CIRCUMFERENTIAL COORDINATES, FOLLOWED BY A CONSECUTIVE STRING
C      OF MAJOR-OUTER,MINOR-OUTER,MAJOR-INNER,MINOR-INNER STRESS VALUES
C      FOR EACH OF THE 4 DIFFERENT LOADING CONDITIONS
C
C      MEL MARCUS, DTNSRDC 1843, FEB 1979
C
C
C      DIMENSION Z(19),TITS(1),TITL(8)
C      DIMENSION GPVAL(16),X(18),    NSEEK(4),C1(2,18),C2(2,103),Y(4,4,18)
C      COMMON WORK(3000)
C
1  FORMAT(1H1)
2  FORMAT(13F6.2)
3  FORMAT(12G11.4)
4  FORMAT(8A10)
5  FORMAT(1X,8A10)
7  FORMAT(26I3)
8  FORMAT(I10,8X,3E18.6/(18X,3E18.6,8X))
9  FORMAT(2I3,E16.8)
C
NLOADS=4
NSKIP=7
NVALUS=16
NS=4
NSEEK(1)=6
NSEEK(2)=7
NSEEK(3)=14
NSEEK(4)=15
C
READ (5,9) NPTS
WRITE (6,9) NPTS
DANG=180./NPTS
N1=6*(NPTS-1)+1
C
```

```

C
C      WRITE (6,1)
DO 20 K=1,NLOADS
      WRITE (6,9) K
C
      DO 10 I=1,NSKIP
10 READ (9,4) TITS(1)
C
      DO 20 I=1,NPTS
      READ (9,8) ID,(GPVAL(M),M=1,NVALUS)
      WRITE (6,8) ID,(GPVAL(M),M=1,NVALUS)
      X(I)=(I-.5)*DANG
C
      DO 20 J=1,NS
      N=NSEEK(J)
20 Y(K,J,I)=GPVAL(N)
C
C
C      SCFAC=.001
C
      WRITE (6,1)
      KOUNT=0
      DO 100 K=1,NLOADS
      DO 100 J=1,NS
C
      DO 30 I=1,NPTS
      C1(1,I)=X(I)
30 C1(2,I)=Y(K,J,I)
C
      CALL CRVFIT(C1,2,NPTS,1,1.0,3,0,1,E-6,N1,0,WORK,3000,C2,RMS,IFAIL)
C
      IF (K.NE.1.OR.J.NE.1) GO TO 40
      KOUNT=KOUNT+1
      WRITE (6,7) KOUNT
      READ (5,4) TITS(1)
      WRITE (6,5) TITS(1)
      WRITE (10) TITS(1)
      READ (5,4) (TITL(I),I=1,8)
      WRITE (6,5) (TITL(I),I=1,8)
      WRITE (10) (TITL(I),I=1,8)
      WRITE (6,3) (C1(1,I),I=1,NPTS)
      WRITE (10) (C1(1,I),I=1,NPTS)
      KOUNT=KOUNT+1
      WRITE (6,7) KOUNT
      READ (5,4) TITS(1)
      WRITE (6,5) TITS(1)
      WRITE (10) TITS(1)
      READ (5,4) (TITL(I),I=1,8)
      WRITE (6,5) (TITL(I),I=1,8)
      WRITE (10) (TITL(I),I=1,8)
      WRITE (6,3) (C2(1,I),I=1,N1)
      WRITE (10) (C2(1,I),I=1,N1)
40 CONTINUE
C
      KOUNT=KOUNT+1
      WRITE (6,7) KOUNT
      READ (5,4) TITS(1)
      WRITE (6,5) TITS(1)
      WRITE (10) TITS(1)
      READ (5,4) (TITL(I),I=1,8)
      WRITE (6,5) (TITL(I),I=1,8)

```

```
      WRITE (10) (TITL(I),I=1,8)
      WRITE (6,3) (C1(2,I)*SCFAC,I=1,NPTS)
      WRITE (10) (C1(2,I)*SCFAC,I=1,NPTS)
      KOUNT=KOUNT+1
      WRITE (6,9) KOUNT,IFAIL,RMS
      READ (5,4) TITS(1)
      WRITE (6,5) TITS(1)
      WRITE (10) TITS(1)
      READ (5,4) (TITL(I),I=1,8)
      WRITE (6,5) (TITL(I),I=1,8)
      WRITE (10) (TITL(I),I=1,8)
      WRITE (6,3) (C2(2,I)*SCFAC,I=1,N1)
      WRITE (10) (C2(2,I)*SCFAC,I=1,N1)

C      100 CONTINUE
C
C
C      END
7/8/9 EOR    +*** INPUT DATA (MESH A) FOLLOWS *****
12
PHI-U
PIPE CIRCUMFERENCE (DEGREES)
PHI
PIPE CIRCUMFERENCE (DEGREES)
PRES-UOMJR
NASTRAN MAJOR STRESS AT OUTER STATION 7 DUE TO PRESSURE LOAD
PRES-NOMJR
NASTRAN MAJOR STRESS AT OUTER STATION 7 DUE TO PRESSURE LOAD
***** SHORT AND LONG NAMES FOR 30 MORE CURVES FOLLOW *****
6/7/8/9 EOF
```

APPENDIX E

Listing of NASTRAN Input Data File
for Mesh A

```

NASTRAN CONFIG=6, FILES=(PLT2.NPTP,OPTP,INPT)
ID PIPE,ELBOW
APP DISP
SOL 1,0
TIME 25
$SEQUENCE YES
$GRID=525
$CONFIG=6
CEND
TITLE =STRESS ANALYSIS OF ELBOW ME-1 (ORNL-TM-4834)
MAXLINES=50000
SET 1 * 545008, 545023, 545038, 545053, 545068, 545083, 545098, 545113,
      54513, 545143, 545158, 545173,
      999999
DISP=ALL
STRESSPRINT,PUNCH)=1
SPCFORCE=ALL
$      SUBCASES HAVING SAME B.C. ARE GROUPED TOGETHER
$      TO AVOID UNNECESSARY MATRIX DECOMPOSITIONS
$SUBCASE 1
SUBTITLE=UNIT PRESSURE LOAD
LABEL=SYM B.C.
LOAD=21
SPC=91
OLOAD=ALL
STRESS=1
$SUBCASE 2
SUBTITLE=INIT IN-PLANE (Z) MOMENT
LABEL=SYM B.C.
LOAD=22
SPC=91
OLOAD=ALL
STRESS=1
$SUBCASE 3
SUBTITLE=UNIT OUT-OF-PLANE (X) MOMENT
LABEL=ANTI-SYM B.C.
LOAD=23
SPC=92
OLOAD=ALL
STRESS=1
$SUBCASE 4
SUBTITLE=UNIT TORSIONAL (Y) MOMENT
LABEL=ANTI-SYM B.C.
LOAD=24
SPC=92
OLOAD=ALL
STRESS=1
$SUBCOM 21
SUBTITLE=PRESSURE LOAD OF 75.53 PSI
SUBSEQ=75.53,0,0,0,0
$SUBCOM 22

```

```

SUBTITLE=IN-PLANE MOMENT OF 32660 IN-LB
SUBSEQ=0...-32660 .0 .0 .
SUBCON 23
SUBTITLE=OUT-OF-PLANE MOMENT OF 32660 IN-LB
SUBSEQ=0 .0 .32660 .0 .
SUBCON 24
SUBTITLE=TORSIONAL MOMENT OF 32660 IN-LB
SUBSEQ=0 .0 .0 .32660 .

$      STRUCTURE    ...PIPE (RPIPE=5.163) CONSISTS OF
$          90 DEGREE ELBOW (RBEND=15.0)
$          ADJOINED BY STRAIGHT SECTIONS

$      SYMMETRY    ...IMPOSED AT PIPE HALF-CIRCUM (PHI=0,180)

$      COORD SYSTEMS... (ELBOW) R=RBEND-RPIPE+COS(PHI)
$                           T=THETA, (THETA=0,90 AT P.C.,P.T.)
$                           Z=RPIPE*SIN(PHI)

$      COORD SYSTEMS... (STRAIGHT SEC) R=RPIPE
$                           T=PHI
$                           (TOP) Z=DISTANCE FROM P.C.
$                           (BOTTOM) Z=DISTANCE FROM P.T.

$      NODAL VALUES ... (ELBOW) ID=1000*(500+ITH)+IPH
$                           WHERE ITH ARE ROUNDED NODAL VALUES OF THETA
$                           IPH ARE ROUNDED NODAL VALUES OF PHI

$      (STRAIGHT SEC) (TOP) ID=1000*(500-10*(J-I))+IPH
$                           I=0,1,2,...,J-1
$                           (BOTTOM) ID=1000*(590+10*I)+IPH
$                           I=1,2,...,K
$                           WHERE J IS NO. OF Z-INTERVALS SUBDIVIDING TOP SEC
$                           K IS NO. OF Z-INTERVALS SUBDIVIDING BOT SEC

$      BEGIN BULK
$      SPOKES AT ELBOW ENDS CONVERGE TO MYTHICAL CENTER POINTS

$      CBAR 500501 201 500000 500500 0.0 1.0 0.0 1
$      CBAR 500502 202 500015 500500 0.0 1.0 0.0 1
$      CBAR 500503 202 500030 500500 0.0 1.0 0.0 1
$      CBAR 500504 202 500045 500500 0.0 1.0 0.0 1
$      CBAR 500505 202 500060 500500 0.0 1.0 0.0 1
$      CBAR 500506 202 500075 500500 0.0 1.0 0.0 1
$      CBAR 500507 202 500090 500500 0.0 1.0 0.0 1
$      CBAR 500508 202 500105 500500 0.0 1.0 0.0 1
$      CBAR 500509 202 500120 500500 0.0 1.0 0.0 1
$      CBAR 500510 202 500135 500500 0.0 1.0 0.0 1
$      CBAR 500511 202 500150 500500 0.0 1.0 0.0 1

```

		ELEMENT CONGRUENCY... (ELBCW)		THETA DIRECTION ONLY	
		(STRAIGHT SEC) BOTH DIRECTIONS			
\$	CNGRNT	390000	390015		
\$	CNGRNT	390000	390030		
\$	CNGRNT	390000	390045		
\$	CNGRNT	390000	390050		
\$	CNGRNT	390000	390075		
\$	CNGRNT	390000	390090		
\$	CNGRNT	390000	390105		
\$	CNGRNT	390000	390120		
\$	CNGRNT	390000	390135		
\$	CNGRNT	390000	390150		
\$	CNGRNT	390000	390165		
\$	CNGRNT	400000	400015		
\$	CNGRNT	400000	400030		
\$	CNGRNT	400000	400045		
\$	CNGRNT	400000	400060		
\$	CNGRNT	400000	400075		
\$	CNGRNT	400000	400090		
\$	CNGRNT	400000	400105		
\$	CNGRNT	400000	400120		
\$	CNGRNT	400000	400135		
\$	CNGRNT	400000	400150		
\$	CNGRNT	400000	400165		
\$	CNGRNT	400000	410000		
\$	CNGRNT	400000	410015		
\$	CNGRNT	400000	410030		
\$	CNGRNT	400000	410045		
\$	CNGRNT	400000	410060		
\$	CNGRNT	400000	410075		
\$	CNGRNT	400000	410090		
\$	CNGRNT	400000	4101C5		
\$	CNGRNT	400000	410120		
\$	CNGRNT	400000	410135		
\$	CNGRNT	400000	410150		
\$	CNGRNT	400000	410165		
\$	CNGRNT	400000	420000		

CNGRNT	400000	420015	DATA 163
CNGRNT	400000	420030	DATA 164
CNGRNT	400000	420045	DATA 165
CNGRNT	400000	420060	DATA 166
CNGRNT	400000	420075	DATA 167
CNGRNT	400000	420090	DATA 168
CNGRNT	400000	420105	DATA 169
CNGRNT	400000	420120	DATA 170
CNGRNT	400000	420135	DATA 171
CNGRNT	400000	420150	DATA 172
CNGRNT	400000	420165	DATA 173
CNGRNT	400000	430000	DATA 174
CNGRNT	400000	430015	DATA 175
CNGRNT	400000	430030	DATA 176
CNGRNT	400000	430045	DATA 177
CNGRNT	400000	430060	DATA 178
CNGRNT	400000	430075	DATA 179
CNGRNT	400000	430090	DATA 180
CNGRNT	400000	430105	DATA 181
CNGRNT	400000	430120	DATA 182
CNGRNT	400000	430135	DATA 183
CNGRNT	400000	430150	DATA 184
CNGRNT	400000	430165	DATA 185
CNGRNT	400000	440000	DATA 186
CNGRNT	400000	440015	DATA 187
CNGRNT	400000	440030	DATA 188
CNGRNT	400000	440045	DATA 189
CNGRNT	400000	440165	DATA 190
CNGRNT	400000	440005	DATA 191
CNGRNT	400000	440020	DATA 192
CNGRNT	400000	440035	DATA 193
CNGRNT	400000	440050	DATA 194
CNGRNT	400000	440065	DATA 195
CNGRNT	400000	440080	DATA 196
CNGRNT	400000	440105	DATA 197
CNGRNT	400000	440120	DATA 198
CNGRNT	400000	440135	DATA 199
CNGRNT	400000	440150	DATA 200
CNGRNT	400000	450005	DATA 201
CNGRNT	400000	450020	DATA 202
CNGRNT	400000	450035	DATA 203
CNGRNT	400000	450050	DATA 204
CNGRNT	400000	450065	DATA 205
CNGRNT	400000	450080	DATA 206
CNGRNT	400000	450105	DATA 207
CNGRNT	400000	450120	DATA 208
CNGRNT	400000	460030	DATA 209
CNGRNT	400000	460045	DATA 210
CNGRNT	400000	460060	DATA 211
CNGRNT	400000	460075	DATA 212
CNGRNT	400000	460090	DATA 213
CNGRNT	400000	460005	DATA 214
CNGRNT	400000	460020	DATA 215
CNGRNT	400000	460035	DATA 216

CNGRNT	400000	460105	DATA	218
CNGRNT	400000	460120	DATA	219
CNGRNT	400000	460135	DATA	220
CNGRNT	400000	460150	DATA	221
CNGRNT	400000	460165	DATA	222
CNGRNT	400000	470000	DATA	223
CNGRNT	400000	470015	DATA	223
CNGRNT	400000	470030	DATA	224
CNGRNT	400000	470045	DATA	225
CNGENT	400000	470060	DATA	226
CNGRNT	400000	470075	DATA	227
CNGRNT	400000	470090	DATA	228
CNGRNT	400000	470105	DATA	229
CNGRNT	400000	470120	DATA	230
CNGRNT	400000	470135	DATA	231
CNGRNT	400000	470150	DATA	232
CNGRNT	400000	470165	DATA	233
CNGRNT	400000	480015	DATA	234
CNGRNT	400000	480030	DATA	235
CNGRNT	400000	480045	DATA	236
CNGRNT	400000	480060	DATA	237
CNGRNT	400000	480075	DATA	238
CNGRNT	400000	480090	DATA	239
CNGRNT	400000	480105	DATA	240
CNGRNT	400000	480120	DATA	241
CNGRNT	400000	480135	DATA	242
CNGRNT	400000	480150	DATA	243
CNGRNT	480000	480165	DATA	244
CNGRNT	503008	508008	DATA	245
CNGRNT	503008	513008	DATA	246
CNGRNT	503008	519008	DATA	247
CNGRNT	503008	524008	DATA	248
CNGRNT	503008	529008	DATA	249
CNGRNT	503008	534008	DATA	250
CNGRNT	503008	540008	DATA	251
CNGRNT	503008	545008	DATA	252
CNGRNT	503008	550008	DATA	253
CNGRNT	503008	556008	DATA	254
CNGRNT	503008	561008	DATA	255
CNGRNT	503008	566008	DATA	256
CNGRNT	503008	571008	DATA	257
CNGRNT	503008	577008	DATA	258
CNGRNT	503008	582008	DATA	259
CNGRNT	503008	587008	DATA	260
CNGRNT	503023	508023	DATA	261
CNGRNT	503023	513023	DATA	262
CNGRNT	503023	519023	DATA	263
CNGRNT	503023	524023	DATA	264
CNGRNT	503023	529023	DATA	265
CNGRNT	503023	534023	DATA	266
CNGRNT	503023	540023	DATA	267
CNGRNT	503023	545023	DATA	268
CNGRNT	503023	550023	DATA	269
CNGRNT	503023	556023	DATA	270

CNGRNT	5C3023	561053	DATA 271
CNGRNT	503023	566023	DATA 272
CNGRNT	503023	571023	DATA 273
CNGRNT	503023	577023	DATA 274
CNGRNT	503023	582023	DATA 275
CNGRNT	503023	587023	DATA 276
CNGRNT	503039	508038	DATA 277
CNGRNT	503038	513038	DATA 278
CNGRNT	503038	519038	DATA 279
CNGRNT	503038	524038	DATA 280
CNGRNT	503038	529038	DATA 281
CNGRNT	503038	534038	DATA 282
CNGRNT	503038	540038	DATA 283
CNGRNT	503038	545038	DATA 284
CNGRNT	503038	550038	DATA 285
CNGRNT	503038	555038	DATA 286
CNGRNT	503038	561038	DATA 287
CNGRNT	503038	566038	DATA 288
CNGRNT	503038	571038	DATA 289
CNGRNT	503038	577038	DATA 290
CNGRNT	503038	582038	DATA 291
CNGRNT	503038	587038	DATA 292
CNGRNT	503053	508053	DATA 293
CNGRNT	503053	513053	DATA 294
CNGRNT	503053	519053	DATA 295
CNGRNT	503053	524053	DATA 296
CNGRNT	503053	529053	DATA 297
CNGRNT	503053	534053	DATA 298
CNGRNT	503053	540053	DATA 299
CNGRNT	503053	545053	DATA 300
CNGRNT	503053	550053	DATA 301
CNGRNT	503053	556053	DATA 302
CNGRNT	503053	561053	DATA 303
CNGRNT	503053	566053	DATA 304
CNGRNT	503053	571053	DATA 305
CNGRNT	503053	577053	DATA 306
CNGRNT	503053	582053	DATA 307
CNGRNT	503053	587053	DATA 308
CNGRNT	503068	508068	DATA 309
CNGRNT	503068	513068	DATA 310
CNGRNT	503068	519068	DATA 311
CNGRNT	503068	524068	DATA 312
CNGRNT	503068	529068	DATA 313
CNGRNT	503068	534068	DATA 314
CNGRNT	503068	540068	DATA 315
CNGRNT	503068	545068	DATA 316
CNGRNT	503068	550068	DATA 317
CNGRNT	503068	556068	DATA 318
CNGRNT	503068	561068	DATA 319
CNGRNT	503068	566068	DATA 320
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CNGRNT	503068	577068	DATA 322
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$      S      ELBOW DEFINED IN COORD SYSTEM 1
$      S      STRAIGHT BOTTOM DEFINED IN COORD SYSTEM 2
$      S      STRAIGHT TOP DEFINED IN COORD SYSTEM 3
$      S      ORNL CARTESIAN SYSTEM IS NO. 4
$      S      CORD2C   1.      0.      0.      0.      0.      1.
$      S      +COR1     1.      0.      0.      0.      0.      +COR1
$      S      CORD2C   2.      0.      0.      15.     -1.      0.
$      S      +COR2     0.      14.     0.      0.      15.     0.
$      S      CORD2C   3.      0.      15.     0.      0.      1.
$      S      +COR3     14.     0.      0.      0.      0.      +COR3
$      S      CORD2R   4.      0.      0.      0.      0.      -1.
$      S      +COR4     1.      0.      0.      0.      0.      +COR4
$      S      FINITE ELEMENT PLATING
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$      S      CQUAD2   400150  200    400150  410150  410165  400165

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				574075	569075

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CQUAD2	680090	200	680090	690090	690105	680105	DATA	1022
CQUAD2	680105	200	680105	690105	690120	680120	DATA	1023
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CQUADD2    690165    200    690165    700165    700165    700165    DATA 1039
$      RIGID CONNECTION FOR FREE ( LOADED ) END OF PIPE
$      CRIGD1   1     2000500  100500  DATA 1040
$      CRIGD1   2     2000500  390000  DATA 1041
$      CRIGD1   3     2000500  3900015 DATA 1042
$      CRIGD1   4     2000500  3900030 DATA 1043
$      CRIGD1   5     2000500  3900045 DATA 1044
$      CRIGD1   6     2000500  3900060 DATA 1045
$      CRIGD1   7     2000500  3900075 DATA 1046
$      CRIGD1   8     2000500  3900090 DATA 1047
$      CRIGD1   9     2000500  3900105 DATA 1048
$      CRIGD1  10    2000500  3900120 DATA 1049
$      CRIGD1  11    2000500  3900135 DATA 1050
$      CRIGD1  12    2000500  3900150 DATA 1051
$      CRIGD1  13    2000500  3900165 DATA 1052
$      CRIGD1  14    2000500  3900180 DATA 1053
$      END CAP LOAD DUE TO UNIT INTERNAL PRESSURE
$      FORCE    21    2000500  3 41.3954  0.  0.  -1.
$      GRID POINTS
$      MYTHICAL CENTER POINT 1 UNIT BEYOND FREE END OF PIPE
$      GRID    100500  0  15.0  -22.0  0.  4
$      MYTHICAL CENTER POINT AT FREE END OF PIPE
$      GRID    2000500  0  15.0  -21.0  0.  4
$      STRAIGHT SECTION ABOVE THETA=0
$      GRID    3000000  3  5.1630  0.000-21.0000 3
$      GRID    390015  3  5.1630  15.000-21.0000 3
$      GRID    390030  3  5.1630  30.000-21.0000 3
$      GRID    390045  3  5.1630  45.000-21.0000 3
$      GRID    390060  3  5.1630  60.000-21.0000 3
$      GRID    390075  3  5.1630  75.000-21.0000 3
$      GRID    390090  3  5.1630  90.000-21.0000 3

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GRID	390135	3	5.1630	135.000-21.0000	3	3	DATA 1083
GRID	390150	3	5.1630	150.000-21.0000	3	3	DATA 1084
GRID	390165	3	5.1630	165.000-21.0000	3	3	DATA 1085
GRID	390180	3	5.1630	180.000-21.0000	3	3	DATA 1086
GRID	400000	3	5.1630	0.000-18.5C00	3	3	DATA 1087
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GRID	400030	3	5.1630	30.000-18.5C00	3	3	DATA 1089
GRID	400045	3	5.1630	45.000-18.5C00	3	3	DATA 1090
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GRID	400090	3	5.1630	90.000-18.5C00	3	3	DATA 1093
GRID	400105	3	5.1630	105.000-18.5C00	3	3	DATA 1094
GRID	400120	3	5.1630	120.000-18.5C00	3	3	DATA 1095
GRID	400135	3	5.1630	135.000-18.5000	3	3	DATA 1096
GRID	400150	3	5.1630	150.000-18.5000	3	3	DATA 1097
GRID	400165	3	5.1630	165.000-18.5000	3	3	DATA 1098
GRID	400180	3	5.1630	180.000-18.5000	3	3	DATA 1099
GRID	410000	3	5.1630	0.000-16.5C00	3	3	DATA 1100
GRID	410015	3	5.1630	15.000-16.5000	3	3	DATA 1101
GRID	410030	3	5.1630	30.000-16.5000	3	3	DATA 1102
GRID	410045	3	5.1630	45.000-16.5000	3	3	DATA 1103
GRID	410060	3	5.1630	60.000-16.5000	3	3	DATA 1104
GRID	410075	3	5.1630	75.000-16.5000	3	3	DATA 1105
GRID	410090	3	5.1630	90.000-16.5000	3	3	DATA 1106
GRID	410105	3	5.1630	105.000-16.5C00	3	3	DATA 1107
GRID	410120	3	5.1630	120.000-16.5C00	3	3	DATA 1108
GRID	410135	3	5.1630	135.000-16.5000	3	3	DATA 1109
GRID	410150	3	5.1630	150.000-16.5000	3	3	DATA 1110
GRID	410165	3	5.1630	165.000-16.5C00	3	3	DATA 1111
GRID	410180	3	5.1630	180.000-16.5C00	3	3	DATA 1112
GRID	420000	3	5.1630	0.000-14.5C00	3	3	DATA 1113
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GRID	420030	3	5.1630	30.000-14.5000	3	3	DATA 1115
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GRID	420060	3	5.1630	60.000-14.5000	3	3	DATA 1117
GRID	420075	3	5.1630	75.000-14.5000	3	3	DATA 1118
GRID	420090	3	5.1630	90.000-14.5000	3	3	DATA 1119
GRID	420105	3	5.1630	105.000-14.5C00	3	3	DATA 1120
GRID	420120	3	5.1630	120.000-14.5C00	3	3	DATA 1121
GRID	420135	3	5.1630	135.000-14.5000	3	3	DATA 1122
GRID	420150	3	5.1630	150.000-14.5000	3	3	DATA 1123
GRID	420165	3	5.1630	165.000-14.5000	3	3	DATA 1124
GRID	420180	3	5.1630	180.000-14.5000	3	3	DATA 1125
GRID	430000	3	5.1630	0.000-12.5000	3	3	DATA 1126
GRID	430015	3	5.1630	15.000-12.5000	3	3	DATA 1127
GRID	430030	3	5.1630	30.000-12.5000	3	3	DATA 1128
GRID	430045	3	5.1630	45.000-12.5000	3	3	DATA 1129
GRID	430060	3	5.1630	60.000-12.5000	3	3	DATA 1130
GRID	430075	3	5.1630	75.000-12.5000	3	3	DATA 1131
GRID	430090	3	5.1630	90.000-12.5000	3	3	DATA 1132
GRID	430105	3	5.1630	105.000-12.5000	3	3	DATA 1133
GRID	430120	3	5.1630	120.000-12.5000	3	3	DATA 1134

GRID	450135	5.1630	135.000-12.5C00	3	DATA 1135
GRID	430150	3.5.1630	150.000-12.5000	3	DATA 1136
GRID	430165	3.5.1E30	165.000-12.5C00	3	DATA 1137
GRID	430180	3.5.1630	180.000-12.5000	3	DATA 1138
GRID	440000	3.5.1630	0.000-10.5000	3	DATA 1139
GRID	440015	3.5.1630	15.000-10.5000	3	DATA 1140
GRID	440030	3.5.1630	30.000-10.5000	3	DATA 1141
GRID	440045	3.5.1630	45.000-10.5000	3	DATA 1142
GRID	440060	3.5.1630	60.000-10.5000	3	DATA 1143
GRID	440075	3.5.1630	75.000-10.5000	3	DATA 1144
GRID	440090	3.5.1630	90.000-10.5000	3	DATA 1145
GRID	440105	3.5.1630	105.000-10.5000	3	DATA 1146
GRID	440120	3.5.1630	120.000-10.5000	3	DATA 1147
GRID	440135	3.5.1630	135.000-10.5000	3	DATA 1148
GRID	440150	3.5.1630	150.000-10.5000	3	DATA 1149
GRID	440165	3.5.1630	165.000-10.5000	3	DATA 1150
GRID	440180	3.5.1630	180.000-10.5000	3	DATA 1151
GRID	450000	3.5.1630	0.000 -8.5C00	3	DATA 1152
GRID	450015	3.5.1630	15.000 -8.5030	3	DATA 1153
GRID	450030	3.5.1630	30.000 -8.5000	3	DATA 1154
GRID	450045	3.5.1630	45.000 -8.5030	3	DATA 1155
GRID	450060	3.5.1630	60.000 -8.5000	3	DATA 1156
GRID	450075	3.5.1630	75.000 -8.5020	3	DATA 1157
GRID	450090	3.5.1630	90.000 -8.5010	3	DATA 1158
GRID	450105	3.5.1630	105.000 -8.5000	3	DATA 1159
GRID	450120	3.5.1630	120.000 -8.5000	3	DATA 1160
GRID	450135	3.5.1630	135.000 -8.5000	3	DATA 1161
GRID	450150	3.5.1630	150.000 -8.5000	3	DATA 1162
GRID	450165	3.5.1630	165.000 -8.5000	3	DATA 1163
GRID	450180	3.5.1630	180.000 -8.5000	3	DATA 1164
GRID	460000	3.5.1630	0.000 -6.5000	3	DATA 1165
GRID	460015	3.5.1630	15.000 -6.5000	3	DATA 1166
GRID	460030	3.5.1630	30.000 -6.5000	3	DATA 1167
GRID	460045	3.5.1630	45.000 -6.5000	3	DATA 1168
GRID	460060	3.5.1630	60.000 -6.5000	3	DATA 1169
GRID	460075	3.5.1630	75.000 -6.5000	3	DATA 1170
GRID	460090	3.5.1630	90.000 -6.5000	3	DATA 1171
GRID	460105	3.5.1630	105.000 -6.5000	3	DATA 1172
GRID	460120	3.5.1630	120.000 -6.5000	3	DATA 1173
GRID	460135	3.5.1630	135.000 -6.5000	3	DATA 1174
GRID	460150	3.5.1630	150.000 -6.5000	3	DATA 1175
GRID	460165	3.5.1630	165.000 -6.5000	3	DATA 1176
GRID	460180	3.5.1630	180.000 -6.5000	3	DATA 1177
GRID	470000	3.5.1630	0.000 -4.5000	3	DATA 1178
GRID	470015	3.5.1630	15.000 -4.5000	3	DATA 1179
GRID	470030	3.5.1630	30.000 -4.5000	3	DATA 1180
GRID	470045	3.5.1630	45.000 -4.5000	3	DATA 1181
GRID	470060	3.5.1630	60.000 -4.5000	3	DATA 1182
GRID	470075	3.5.1630	75.000 -4.5000	3	DATA 1183
GRID	470090	3.5.1630	90.000 -4.5000	3	DATA 1184
GRID	470105	3.5.1630	105.000 -4.5000	3	DATA 1185
GRID	470120	3.5.1630	120.000 -4.5000	3	DATA 1186
GRID	470135	3.5.1630	135.000 -4.5000	3	DATA 1187
GRID	470150	3.5.1630	150.000 -4.5000	3	DATA 1188

GRID	505075	1	13.6637	5.294	4.9871	1243
GRID	505090	1	15.0000	5.294	5.1630	DATA
GRID	505105	1	16.3363	5.294	4.9871	1244
GRID	505120	1	17.5815	5.294	4.4713	DATA
GRID	505135	1	18.6508	5.294	3.6508	1245
GRID	505150	1	19.4713	5.294	2.5615	DATA
GRID	505165	1	19.9971	5.294	1.3363	1246
GRID	505180	1	20.1630	5.294	-0.0000	DATA
GRID	511000	1	9.8370	10.588	0.0000	1247
GRID	511015	1	10.0129	10.588	1.3363	DATA
GRID	511030	1	10.5287	10.588	2.5315	1248
GRID	511045	1	11.3492	10.588	3.6624	DATA
GRID	511060	1	12.4185	10.588	4.4713	1249
GRID	511075	1	13.6637	10.588	4.9871	DATA
GRID	511090	1	15.0000	10.588	5.1630	1250
GRID	511105	1	16.3363	10.588	4.9871	DATA
GRID	511120	1	17.5815	10.588	4.4713	1251
GRID	511135	1	18.6508	10.588	3.6508	DATA
GRID	511150	1	19.4713	10.588	2.5615	1252
GRID	511165	1	19.9971	10.588	1.3363	DATA
GRID	511180	1	20.1630	10.588	-0.0000	1253
GRID	516030	1	9.8370	15.882	0.0000	DATA
GRID	516015	1	10.0129	15.882	1.3363	1254
GRID	516030	1	10.5287	15.882	2.5815	DATA
GRID	516045	1	11.3492	15.882	3.6508	1255
GRID	516060	1	12.4185	15.882	4.4713	DATA
GRID	516075	1	13.6637	15.882	4.9871	1256
GRID	516090	1	15.0000	15.882	5.1630	DATA
GRID	516105	1	16.3363	15.882	4.9871	1260
GRID	516120	1	17.5815	15.882	4.4713	DATA
GRID	516135	1	18.6508	15.882	3.6508	1261
GRID	516150	1	19.4713	15.882	2.5815	DATA
GRID	516165	1	19.9971	15.882	1.3363	1262
GRID	516180	1	20.1630	15.882	-0.0000	1263
GRID	521000	1	9.8370	21.176	0.0000	DATA
GRID	521015	1	10.0129	21.176	1.3363	1264
GRID	521030	1	10.5287	21.176	2.5615	DATA
GRID	521045	1	11.3492	21.176	3.6508	1265
GRID	521060	1	12.4185	21.176	4.4713	DATA
GRID	521075	1	13.6637	21.176	4.9871	1266
GRID	521090	1	15.0000	21.176	5.1630	DATA
GRID	521105	1	16.3363	21.176	4.9871	1267
GRID	521120	1	17.5815	21.176	4.4713	DATA
GRID	521135	1	18.6508	21.176	3.6508	1268
GRID	521150	1	19.4713	21.176	2.5615	DATA
GRID	521165	1	19.9971	21.176	1.3363	1269
GRID	521180	1	20.1630	21.176	-0.0000	DATA
GRID	526000	1	9.8370	26.471	0.0000	1270
GRID	526015	1	10.0129	26.471	1.3363	DATA
GRID	526030	1	10.5287	26.471	2.5815	1271
GRID	526045	1	11.3492	26.471	3.6508	DATA
GRID	526060	1	12.4185	26.471	4.4713	1272
GRID	526075	1	13.6637	26.471	4.9871	DATA
GRID	526090	1	15.0000	26.471	5.1630	1273

GRID	526105	16.3363	26.471	4.9671	1	DATA 1257
GRID	526120	17.5815	26.471	4.4713	1	DATA 1258
GRID	526135	18.6508	26.471	3.6508	1	DATA 1259
GRID	526150	19.4713	26.471	2.5615	1	DATA 1300
GRID	526165	19.9871	26.471	1.363	1	DATA 1301
GRID	526180	20.-630	26.471	-0.000	1	DATA 1302
GRID	532000	9.8370	31.765	0.000	1	DATA 1303
GRID	532015	10.0129	31.765	1.3363	1	DATA 1304
GRID	532030	10.5287	31.765	2.5615	1	DATA 1305
GRID	532045	11.3492	31.765	3.6508	1	DATA 1306
GRID	532060	12.4185	31.765	4.4713	1	DATA 1307
GRID	532075	13.6637	31.765	4.9E71	1	DATA 1308
GRID	532090	15.0000	31.765	5.1630	1	DATA 1309
GRID	532105	16.3363	31.765	4.9871	1	DATA 1310
GRID	532120	17.5815	31.765	4.4713	1	DATA 1311
GRID	532135	18.6508	31.765	3.6508	1	DATA 1312
GRID	532150	19.4713	31.765	2.5615	1	DATA 1313
GRID	532165	19.9871	31.765	1.3363	1	DATA 1314
GRID	532180	20.1630	31.765	-0.000	1	DATA 1315
GRID	537000	9.8370	37.059	0.000	1	DATA 1316
GRID	537015	10.0129	37.059	1.3353	1	DATA 1317
GRID	537030	10.5287	37.059	2.5615	1	DATA 1318
GRID	537045	11.3492	37.059	3.6508	1	DATA 1319
GRID	537060	12.4185	37.059	4.4713	1	DATA 1320
GRID	537075	13.6637	37.059	4.9671	1	DATA 1321
GRID	537090	15.0000	37.059	5.1E30	1	DATA 1322
GRID	537105	16.3363	37.059	4.5E71	1	DATA 1323
GRID	537120	17.5815	37.059	4.4713	1	DATA 1324
GRID	537135	18.6508	37.059	3.6508	1	DATA 1325
GRID	537150	19.4713	37.059	2.5615	1	DATA 1326
GRID	537165	19.9871	37.059	1.3353	1	DATA 1327
GRID	537180	20.1630	37.059	-0.000	1	DATA 1328
GRID	542000	9.8370	42.353	0.000	1	DATA 1329
GRID	542015	10.0129	42.353	1.3363	1	DATA 1330
GRID	542030	10.5287	42.353	2.5615	1	DATA 1331
GRID	542045	11.3492	42.353	3.6508	1	DATA 1332
GRID	542060	12.4185	42.353	4.4713	1	DATA 1333
GRID	542075	13.6637	42.353	4.9671	1	DATA 1334
GRID	542090	15.0000	42.353	5.1E30	1	DATA 1335
GRID	542105	16.3363	42.353	4.9671	1	DATA 1336
GRID	542120	17.5815	42.353	4.4713	1	DATA 1337
GRID	542135	18.6508	42.353	3.6508	1	DATA 1338
GRID	542150	19.4713	42.353	2.5815	1	DATA 1339
GRID	542165	19.9871	42.353	1.3363	1	DATA 1340
GRID	542180	20.1630	42.353	-0.000	1	DATA 1341
GRID	548000	9.8370	47.647	0.000	1	DATA 1342
GRID	548015	10.0129	47.647	1.3363	1	DATA 1343
GRID	548030	10.5287	47.647	2.5815	1	DATA 1344
GRID	548045	11.3492	47.647	3.6508	1	DATA 1345
GRID	548060	12.4185	47.647	4.4713	1	DATA 1346
GRID	548075	13.6637	47.647	4.9671	1	DATA 1347
GRID	548090	15.0000	47.647	5.1E30	1	DATA 1348
GRID	548105	16.3363	47.647	4.9871	1	DATA 1349
GRID	548120	17.5815	47.647	4.4713	1	DATA 1350

GRID	548135	1	18.6508	47.647	3.6508	DATA 1351
GRID	548150	1	19.4713	47.647	2.5015	DATA 1352
GRID	548165	1	19.9871	47.647	1.3363	DATA 1353
GRID	548180	1	20.1630	47.647	-0.0000	DATA 1354
GRID	553000	1	9.8370	52.941	0.0000	DATA 1355
GRID	553015	1	10.0129	52.941	1.3363	DATA 1356
GRID	553030	1	10.5287	52.941	2.5615	DATA 1357
GRID	553045	1	11.3492	52.941	3.6508	DATA 1358
GRID	553060	1	12.4185	52.941	4.4713	DATA 1359
GRID	553075	1	13.6637	52.941	4.9671	DATA 1360
GRID	553090	1	15.0000	52.941	5.1630	DATA 1361
GRID	553105	1	16.3363	52.941	4.9871	DATA 1362
GRID	553120	1	17.5815	52.941	4.4713	DATA 1363
GRID	553135	1	18.6508	52.941	3.6508	DATA 1364
GRID	553150	1	19.4713	52.941	2.5815	DATA 1365
GRID	553165	1	19.9871	52.941	1.3363	DATA 1366
GRID	553180	1	20.1630	52.941	-0.0000	DATA 1367
GRID	558000	1	9.8370	58.235	0.0000	DATA 1368
GRID	558015	1	10.0129	58.235	1.3363	DATA 1369
GRID	558030	1	10.5287	58.235	2.5815	DATA 1370
GRID	558045	1	11.3492	58.235	3.6508	DATA 1371
GRID	558060	1	12.4185	58.235	4.4713	DATA 1372
GRID	558075	1	13.6637	58.235	4.9871	DATA 1373
GRID	558090	1	15.0000	58.235	5.1630	DATA 1374
GRID	558105	1	16.3363	58.235	4.9871	DATA 1375
GRID	558120	1	17.5815	58.235	4.4713	DATA 1376
GRID	558135	1	18.6508	58.235	3.6508	DATA 1377
GRID	558150	1	19.4713	58.235	2.5815	DATA 1378
GRID	558165	1	19.9871	58.235	1.3363	DATA 1379
GRID	558180	1	20.1630	58.235	-0.0000	DATA 1380
GRID	564000	1	9.8370	63.529	0.0000	DATA 1381
GRID	564015	1	10.0129	63.529	1.3363	DATA 1382
GRID	564030	1	10.5287	63.529	2.5815	DATA 1383
GRID	564045	1	11.3492	63.529	3.6508	DATA 1384
GRID	564060	1	12.4185	63.529	4.4713	DATA 1385
GRID	564075	1	13.6637	63.529	4.9871	DATA 1386
GRID	564090	1	15.0000	63.529	5.1630	DATA 1387
GRID	564105	1	16.3363	63.529	4.9371	DATA 1388
GRID	564120	1	17.5815	63.529	4.4713	DATA 1389
GRID	564135	1	18.6508	63.529	3.6508	DATA 1390
GRID	564150	1	19.4713	63.529	2.5815	DATA 1391
GRID	564165	1	19.9871	63.529	1.3363	DATA 1392
GRID	564180	1	20.1630	63.529	-0.0000	DATA 1393
GRID	569000	1	9.8370	68.824	0.0000	DATA 1394
GRID	569015	1	10.0129	68.824	1.3363	DATA 1395
GRID	569030	1	10.5287	68.824	2.5815	DATA 1396
GRID	569045	1	11.3492	68.824	3.6508	DATA 1397
GRID	569060	1	12.4185	68.824	4.4713	DATA 1398
GRID	569075	1	13.6637	68.824	4.9871	DATA 1399
GRID	569090	1	15.0000	68.824	5.1630	DATA 1400
GRID	569105	1	16.3363	68.824	4.9871	DATA 1401
GRID	569120	1	17.5815	68.824	4.4713	DATA 1402
GRID	569135	1	18.6508	68.824	3.6508	DATA 1403
GRID	569150	1	19.4713	68.824	2.5815	DATA 1404

569165	19.9871	68.824	1.3363
GRID	20.1630	68.824	-0.0000
GRID	9.8370	74.118	0.0000
GRID	10.0129	74.118	1.3363
GRID	10.5287	74.118	2.5815
GRID	11.3492	74.118	3.6508
GRID	12.4185	74.118	4.4713
GRID	13.6637	74.118	4.9871
GRID	15.0000	74.118	5.1630
GRID	16.3363	74.118	4.9871
GRID	17.5815	74.118	4.4713
GRID	18.6508	74.118	3.6508
GRID	19.4713	74.118	2.5815
GRID	19.9871	74.118	1.3363
GRID	20.1630	74.118	-0.0000
GRID	9.8370	79.412	0.0000
GRID	10.0129	79.412	1.3363
GRID	10.5287	79.412	2.5815
GRID	11.3492	79.412	3.6508
GRID	12.4185	79.412	4.4713
GRID	13.6637	79.412	4.9871
GRID	15.0000	79.412	5.1630
GRID	16.3363	79.412	4.9871
GRID	17.5815	79.412	4.4713
GRID	18.6508	79.412	3.6508
GRID	19.4713	79.412	2.5815
GRID	19.9871	79.412	1.3363
GRID	20.1630	79.412	-0.0000
GRID	9.8370	79.412	0.0000
GRID	10.0129	79.412	1.3363
GRID	10.5287	79.412	2.5815
GRID	11.3492	79.412	3.6508
GRID	12.4185	79.412	4.4713
GRID	13.6637	79.412	4.9871
GRID	15.0000	79.412	5.1630
GRID	16.3363	79.412	4.9871
GRID	17.5815	79.412	4.4713
GRID	18.6508	79.412	3.6508
GRID	19.4713	79.412	2.5815
GRID	19.9871	79.412	1.3363
GRID	20.1630	79.412	-0.0000
GRID	9.8370	84.706	0.0000
GRID	10.0129	80.000	1.3363
GRID	10.5287	80.000	2.5815
GRID	11.3492	80.000	3.6508
GRID	12.4185	80.000	4.4713
GRID	13.6637	80.000	4.9871
GRID	15.0000	80.000	5.1630
GRID	16.3363	80.000	4.9871
GRID	17.5815	80.000	4.4713
GRID	18.6508	80.000	3.6508
GRID	19.4713	80.000	2.5815
GRID	19.9871	80.000	1.3363
GRID	20.1630	80.000	-0.0000

S S MYTHICAL CENTER POINT AT THETA=90 END OF ELBOW
S S (EQUIV TO ORIGIN OF COORD SYS 2)
GRID 590500 0 0. 15. 0. 4

DATA 1459 DATA 1460
 DATA 1461 DATA 1462
 DATA 1463 DATA 1464
 DATA 1465 DATA 1466
 DATA 1467 DATA 1468
 DATA 1469 DATA 1470
 DATA 1471 DATA 1472
 DATA 1473 DATA 1474
 DATA 1475 DATA 1476
 DATA 1477 DATA 1478
 DATA 1479 DATA 1480
 DATA 1481 DATA 1482
 DATA 1483 DATA 1484
 DATA 1485 DATA 1486
 DATA 1487 DATA 1488
 DATA 1489 DATA 1490
 DATA 1491 DATA 1492
 DATA 1493 DATA 1494
 DATA 1495 DATA 1496
 DATA 1497 DATA 1498
 DATA 1499 DATA 1500
 DATA 1501 DATA 1502
 DATA 1503 DATA 1504
 DATA 1505 DATA 1506
 DATA 1507 DATA 1508
 DATA 1509 DATA 1510
 DATA 1511 DATA 1512

MYTHICAL CENTER POINT AT THETA=90 END OF ELBOW
(EQUIV TO ORIGIN OF COORD SYS 2)
 GRID 590500 0. 15. 4.
S STRAIGHT SECTION BELOW THETA=90

	2	5.1630	0.000	1.0000
GRID	600000	2	5.1630	0.000
GRID	600015	2	5.1630	.5.000
GRID	600030	2	5.1630	30.000
GRID	600045	2	5.1630	45.000
GRID	600060	2	5.1630	50.000
GRID	600075	2	5.1630	75.000
GRID	600090	2	5.1630	90.000
GRID	600105	2	5.1630	105.000
GRID	600120	2	5.1630	120.000
GRID	600135	2	5.1630	135.000
GRID	600150	2	5.1630	150.000
GRID	600165	2	5.1630	165.000
GRID	600180	2	5.1630	180.000
GRID	610000	2	5.1630	0.000
GRID	610015	2	5.1630	15.000
GRID	610030	2	5.1630	30.000
GRID	610045	2	5.1630	45.000
GRID	610060	2	5.1630	60.000
GRID	610075	2	5.1630	75.000
GRID	610090	2	5.1630	90.000
GRID	610105	2	5.1630	105.000
GRID	610120	2	5.1630	120.000
GRID	610135	2	5.1630	135.000
GRID	610150	2	5.1630	150.000
GRID	610165	2	5.1630	165.000
GRID	610180	2	5.1630	180.000
GRID	620000	2	5.1630	0.000
GRID	620015	2	5.1630	15.000
GRID	620030	2	5.1630	30.000
GRID	620045	2	5.1630	45.000
GRID	620060	2	5.1630	60.000
GRID	620075	2	5.1630	75.000
GRID	620090	2	5.1630	90.000
GRID	620105	2	5.1630	105.000
GRID	620120	2	5.1630	120.000
GRID	620135	2	5.1630	135.000
GRID	620150	2	5.1630	150.000
GRID	620165	2	5.1630	165.000
GRID	620180	2	5.1630	180.000
GRID	630000	2	5.1630	0.000
GRID	630015	2	5.1630	15.000
GRID	630030	2	5.1630	30.000
GRID	630045	2	5.1630	45.000
GRID	630060	2	5.1630	60.000
GRID	630075	2	5.1630	75.000
GRID	630090	2	5.1630	90.000
GRID	630105	2	5.1630	105.000

GRID	630120	2	5.1630	120.000	6.5000	DATA 1513
GRID	630135	2	5.1630	135.000	6.5000	DATA 1514
GRID	630150	2	5.1630	150.000	6.5000	DATA 1515
GRID	630165	2	5.1630	165.000	6.5000	DATA 1516
GRID	630180	2	5.1630	180.000	6.5000	DATA 1517
GRID	640000	2	5.1630	0.000	8.5000	DATA 1518
GRID	640015	2	5.1630	15.000	8.5000	DATA 1519
GRID	640030	2	5.1630	30.000	8.5000	DATA 1520
GRID	640045	2	5.1630	45.000	8.5000	DATA 1521
GRID	640060	2	5.1630	60.000	8.5000	DATA 1522
GRID	640075	2	5.1630	75.000	8.5000	DATA 1523
GRID	640090	2	5.1630	90.000	8.5000	DATA 1524
GRID	640105	2	5.1630	105.000	8.5000	DATA 1525
GRID	640120	2	5.1630	120.000	8.5000	DATA 1526
GRID	640135	2	5.1630	135.000	8.5000	DATA 1527
GRID	640150	2	5.1630	150.000	8.5000	DATA 1528
GRID	640165	2	5.1630	165.000	8.5000	DATA 1529
GRID	640180	2	5.1630	180.000	8.5000	DATA 1530
GRID	650000	2	5.1630	0.000	10.5000	DATA 1531
GRID	650015	2	5.1630	15.000	10.5000	DATA 1532
GRID	650030	2	5.1630	30.000	10.5000	DATA 1533
GRID	650045	2	5.1630	45.000	10.5000	DATA 1534
GRID	650060	2	5.1630	60.000	10.5000	DATA 1535
GRID	650075	2	5.1630	75.000	10.5000	DATA 1536
GRID	650090	2	5.1630	90.000	10.5000	DATA 1537
GRID	650105	2	5.1630	105.000	10.5000	DATA 1538
GRID	650120	2	5.1630	120.000	10.5000	DATA 1539
GRID	650135	2	5.1630	135.000	10.5000	DATA 1540
GRID	650150	2	5.1630	150.000	10.5000	DATA 1541
GRID	650165	2	5.1630	165.000	10.5000	DATA 1542
GRID	650180	2	5.1630	180.000	10.5000	DATA 1543
GRID	660000	2	5.1630	0.000	12.5000	DATA 1544
GRID	660015	2	5.1630	15.000	12.5000	DATA 1545
GRID	660030	2	5.1630	30.000	12.5000	DATA 1546
GRID	660045	2	5.1630	45.000	12.5000	DATA 1547
GRID	660060	2	5.1630	60.000	12.5000	DATA 1548
GRID	660075	2	5.1630	75.000	12.5000	DATA 1549
GRID	660090	2	5.1630	90.000	12.5000	DATA 1550
GRID	660105	2	5.1630	105.000	12.5000	DATA 1551
GRID	660120	2	5.1630	120.000	12.5000	DATA 1552
GRID	660135	2	5.1630	135.000	12.5000	DATA 1553
GRID	660150	2	5.1630	150.000	12.5000	DATA 1554
GRID	660165	2	5.1630	165.000	12.5000	DATA 1555
GRID	660180	2	5.1630	180.000	12.5000	DATA 1556
GRID	670000	2	5.1630	0.000	14.5000	DATA 1557
GRID	670015	2	5.1630	15.000	14.5000	DATA 1558
GRID	670030	2	5.1630	30.000	14.5000	DATA 1559
GRID	670045	2	5.1630	45.000	14.5000	DATA 1560
GRID	670060	2	5.1630	60.000	14.5000	DATA 1561
GRID	670075	2	5.1630	75.000	14.5000	DATA 1562
GRID	670090	2	5.1630	90.000	14.5000	DATA 1563
GRID	670105	2	5.1630	105.000	14.5000	DATA 1564
GRID	670120	2	5.1630	120.000	14.5000	DATA 1565
GRID	670135	2	5.1630	135.000	14.5000	DATA 1566

GRID	670150	5.1630	150.000	14.5000		DATA 1567
GRID	670165	5.1630	165.000	14.5000		DATA 1568
GRID	670180	2.2	5.1630	180.000	14.5000	DATA 1569
GRID	680000	2.2	5.1630	0.000	16.5000	DATA 1570
GRID	680015	2.2	5.1630	15.000	16.5000	DATA 1571
GRID	680030	2.2	5.1630	30.000	16.5000	DATA 1572
GRID	680045	2.2	5.1630	45.000	16.5000	DATA 1573
GRID	68C060	2.2	5.1630	60.000	16.5000	DATA 1574
GRID	68C075	2.2	5.1630	75.000	16.5000	DATA 1575
GRID	68C090	2.2	5.1630	90.000	16.5000	DATA 1576
GRID	680105	2.2	5.1630	105.000	16.5000	DATA 1577
GRID	680120	2.2	5.1630	120.000	16.5000	DATA 1578
GRID	680135	2.2	5.1630	135.000	16.5000	DATA 1579
GRID	6d0150	2.2	5.1630	150.000	16.5000	DATA 1580
GRID	680165	2.2	5.1630	165.000	16.5000	DATA 1581
GRID	6BC180	2.2	5.1630	180.000	16.5000	DATA 1582
GRID	690000	2.2	5.1630	0.000	18.5000	DATA 1583
GRID	690015	2.2	5.1630	5.000	18.5000	DATA 1584
GRID	690030	2.2	5.1630	30.000	18.5000	DATA 1585
GRID	690045	2.2	5.1630	45.000	18.5000	DATA 1586
GRID	650060	2.2	5.1630	60.000	18.5000	DATA 1587
GRID	690075	2.2	5.1630	75.000	18.5000	DATA 1588
GRID	690090	2.2	5.1630	90.000	18.5000	DATA 1589
GRID	690105	2.2	5.1630	105.000	18.5000	DATA 1590
GRID	690120	2.2	5.1630	120.000	18.5000	DATA 1591
GRID	690135	2.2	5.1630	135.000	18.5000	DATA 1592
GRID	690150	2.2	5.1630	150.000	18.5000	DATA 1593
GRID	690165	2.2	5.1630	165.000	18.5000	DATA 1594
GRID	690180	2.2	5.1630	180.000	18.5000	DATA 1595
GRID	700000	2.2	5.1630	0.000	20.5000	DATA 1596
GRID	700015	2.2	5.1630	15.000	20.5000	DATA 1597
GRID	700030	2.2	5.1630	30.000	20.5000	DATA 1598
GRID	700045	2.2	5.1630	45.000	20.5000	DATA 1599
GRID	700060	2.2	5.1630	60.000	20.5000	DATA 1600
GRID	700075	2.2	5.1630	75.000	20.5000	DATA 1601
GRID	700090	2.2	5.1630	90.000	20.5000	DATA 1602
GRID	700105	2.2	5.1630	105.000	20.5000	DATA 1603
GRID	700120	2.2	5.1630	120.000	20.5000	DATA 1604
GRID	700135	2.2	5.1630	135.000	20.5000	DATA 1605
GRID	700150	2.2	5.1630	150.000	20.5000	DATA 1606
GRID	700165	2.2	5.1630	165.000	20.5000	DATA 1607
GRID	700180	2.2	5.1630	180.000	20.5000	DATA 1608
\$	MAT1	45	2.9+7	0.3	7.324-4	STEEL
\$	BENDING MOMENTS APPLIED AT FREE END					
\$	MOMENT	22	200500	0	0.50	0.
\$	MOMENT	23	200500	0	0.50	1.
\$	MOMENT	24	200500	0	0.50	0.
\$	PBAR	201	45	1.0-6	1.0-9	1.0-9
\$	PBAR	202	45	2.0-6	2.0-9	2.0-9
\$						4.0-9
\$						DATA 1619
\$						DATA 1620

INTERNAL PRESSURE LOADING FOR PIPE

\$	PLOAD2	21	-1.000	390000		DATA 1621
	PLOAD2	21	-1.000	390015		DATA 1622
	PLOAD2	21	-1.000	390030		DATA 1623
	PLOAD2	21	-1.000	390045		DATA 1624
	PLOAD2	21	-1.000	390060		DATA 1625
	PLOAD2	21	-1.000	390075		DATA 1626
	PLOAD2	21	-1.000	390090		DATA 1627
	PLOAD2	21	-1.000	390105		DATA 1628
	PLOAD2	21	-1.000	390120		DATA 1629
	PLOAD2	21	-1.000	390135		DATA 1630
	PLOAD2	21	-1.000	390150		DATA 1631
	PLOAD2	21	-1.000	390165		DATA 1632
	PLOAD2	21	-1.000	400000		DATA 1633
	PLOAD2	21	-1.000	400015		DATA 1634
	PLOAD2	21	-1.000	400030		DATA 1635
	PLOAD2	21	-1.000	400045		DATA 1636
	PLOAD2	21	-1.000	400060		DATA 1637
	PLOAD2	21	-1.000	400075		DATA 1638
	PLOAD2	21	-1.000	400090		DATA 1639
	PLOAD2	21	-1.000	400105		DATA 1640
	PLOAD2	21	-1.000	400120		DATA 1641
	PLOAD2	21	-1.000	400135		DATA 1642
	PLOAD2	21	-1.000	400150		DATA 1643
	PLOAD2	21	-1.000	400165		DATA 1644
	PLOAD2	21	-1.000	400180		DATA 1645
	PLOAD2	21	-1.000	400195		DATA 1646
	PLOAD2	21	-1.000	410000		DATA 1647
	PLOAD2	21	-1.000	410015		DATA 1648
	PLOAD2	21	-1.000	410030		DATA 1649
	PLOAD2	21	-1.000	410045		DATA 1650
	PLOAD2	21	-1.000	410060		DATA 1651
	PLOAD2	21	-1.000	410075		DATA 1652
	PLOAD2	21	-1.000	410090		DATA 1653
	PLOAD2	21	-1.000	410105		DATA 1654
	PLOAD2	21	-1.000	410120		DATA 1655
	PLOAD2	21	-1.000	410135		DATA 1656
	PLOAD2	21	-1.000	410150		DATA 1657
	PLOAD2	21	-1.000	410165		DATA 1658
	PLOAD2	21	-1.000	420000		DATA 1659
	PLOAD2	21	-1.000	420015		DATA 1660
	PLOAD2	21	-1.000	420030		DATA 1661
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	PLOAD2	21	-1.000	420060		DATA 1663
	PLOAD2	21	-1.000	420075		DATA 1664
	PLOAD2	21	-1.000	420090		DATA 1665
	PLOAD2	21	-1.000	420105		DATA 1666
	PLOAD2	21	-1.000	420120		DATA 1667
	PLOAD2	21	-1.000	420135		DATA 1668
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	PLOAD2	21	-1.000	430015		DATA 1672
	PLOAD2	21	-1.000	430030		DATA 1673
	PLOAD2	21	-1.000	430045		DATA 1674

PLOAD2	21	-1.000	430060	DATA 1675
PLOAD2	21	-1.000	430075	DATA 1676
PLOAD2	21	-1.000	430090	DATA 1677
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PLOAD2	21	-1.000	430150	DATA 1681
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PLOAD2	21	-1.000	440000	DATA 1683
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PLOAD2	21	-1.000	440030	DATA 1685
PLOAD2	21	-1.000	440045	DATA 1686
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PLOAD2	21	-1.000	450000	DATA 1695
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PLOAD2	21	-1.000	513098	DATA 1785
PLOAD2	21	-1.000	513113	DATA 1786
PLOAD2	21	-1.000	513128	DATA 1787
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PLOAD2	21	-1.000	513158	DATA 1789
PLOAD2	21	-1.000	513173	DATA 1790
PLOAD2	21	-1.000	519008	DATA 1791
PLOAD2	21	-1.000	519023	DATA 1792
PLOAD2	21	-1.000	519038	DATA 1793
PLOAD2	21	-1.000	519053	DATA 1794
PLOAD2	21	-1.000	519068	DATA 1795
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PLOAD2	21	-1.000	519158	DATA 1800
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PLOAD2	21	-1.000	550068	DATA 1867
PLOAD2	21	-1.000	550083	DATA 1868
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PLOAD2	21	-1.000	556023	DATA 1876
PLOAD2	21	-1.000	556038	DATA 1877
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PLOAD2	21	-1.000	556113	DATA 1882
PLOAD2	21	-1.000	556128	DATA 1883
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PLOAD2	21	-1.000	556158	DATA 1885
PLOAD2	21	-1.000	556173	DATA 1886
PLOAD2	21	-1.000	561008	DATA 1887
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PLOAD2	21	-1.000	561038	DATA 1889
PLOAD2	21	-1.000	561053	DATA 1890

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PLOAD2	21	-1.000	561098	DATA 1893
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PLOAD2	21	-1.000	561128	DATA 1895
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PLOAD2	21	-1.000	566083	DATA 1904
PLOAD2	21	-1.000	566098	DATA 1905
PLOAD2	21	-1.000	566113	DATA 1906
PLOAD2	21	-1.000	566128	DATA 1907
PLOAD2	21	-1.000	566143	DATA 1908
PLOAD2	21	-1.000	566158	DATA 1909
PLOAD2	21	-1.000	566173	DATA 1910
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PLOAD2	21	-1.000	571128	DATA 1919
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PLOAD2	21	-1.000	571158	DATA 1921
PLOAD2	21	-1.000	571173	DATA 1922
PLOAD2	21	-1.000	577008	DATA 1923
PLOAD2	21	-1.000	577023	DATA 1924
PLOAD2	21	-1.000	577038	DATA 1925
PLOAD2	21	-1.000	577053	DATA 1926
PLOAD2	21	-1.000	577068	DATA 1927
PLOAD2	21	-1.000	577083	DATA 1928
PLOAD2	21	-1.000	577098	DATA 1929
PLOAD2	21	-1.000	577113	DATA 1930
PLOAD2	21	-1.000	577128	DATA 1931
PLOAD2	21	-1.000	577143	DATA 1932
PLOAD2	21	-1.000	582053	DATA 1933
PLOAD2	21	-1.000	582068	DATA 1934
PLOAD2	21	-1.000	582083	DATA 1935
PLOAD2	21	-1.000	582098	DATA 1940
PLOAD2	21	-1.000	582113	DATA 1941
PLOAD2	21	-1.000	582128	DATA 1942
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SPC	71	450180	246	DATA 2108
SPC	71	460000	246	DATA 2109
SPC	71	460180	246	DATA 2110
SPC	71	470000	246	DATA 2111
SPC	71	470180	246	DATA 2112
SPC	71	480000	246	DATA 2113
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SPC	71	490000	246	DATA 2115
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SPC	71	500000	345	DATA 2118
SPC	71	500180	345	DATA 2119
SPC	71	505000	345	DATA 2120
SPC	71	505180	345	DATA 2121
SPC	71	510000	345	DATA 2122
SPC	71	510180	345	DATA 2123
SPC	71	511800	345	DATA 2124
SPC	71	516000	345	DATA 2125
SPC	71	516180	345	DATA 2126
SPC	71	520000	345	DATA 2127
SPC	71	521180	345	DATA 2128
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SPC	71	526180	345	DATA 2130
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SPC	71	548000	345	DATA 2137
SPC	71	548180	345	DATA 2138
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SPC	71	590180	345	DATA 2154
SPC	71	590500	345	DATA 2155
SPC	71	600000	246	DATA 2156
SPC	71	600180	246	DATA 2157
S ² C	71	610000	246	DATA 2158
SPC	71	610180	246	DATA 2159
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SPC	71	620180	246	

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SPC	72	542000	126	DATA 2218
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SPC	72	670000	135	DATA 2253
SPC	72	670180	135	DATA 2254
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SPC	72	680180	135	DATA 2256
SPC	72	690000	135	DATA 2257
SPC	72	690180	135	DATA 2258
SPC	72	700000	135	DATA 2259
SPC	72	700180	135	DATA 2260
SPC	80	420000	4	DATA 2261
SPC	80	400000	4	DATA 2262
SPC	80	400180	4	DATA 2263
SPC	80	410000	4	DATA 2264
SPC	80	410180	4	DATA 2265
SPC	80	420000	4	DATA 2266
SPC	80	420180	4	DATA 2267
SPC	80	430000	4	DATA 2268

\$ ELIMINATION OF ZERO STIFFNESS DOF

CONSTRAIN FIXED END

SPCADD 91 71 80 85
SPCADD 92 72 80 85
ENDDATA

DATA 2323
DATA 2324
DATA 2325

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